A hybrid algorithm for voltage stability enhancement of distribution systems

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ABSTRACT

This paper presents a hybrid algorithm by applying a hybrid firefly and particle swarm optimization algorithm (HFPSO) to determine the optimal sizing of distributed generation (DG) and distribution static compensator (D-STATCOM) device. A multi-objective function is employed to enhance the voltage stability, voltage profile, and minimize the total power loss of the radial distribution system (RDS). Firstly, the voltage stability index (VSI) is applied to locate the optimal location of DG and D-STATCOM respectively. Secondly, to overcome the sup-optimal operation of existing algorithms, the HFPSO algorithm is utilized to determine the optimal size of both DG and D-STATCOM. Verification of the proposed algorithm has achieved on the standard IEEE 33-bus and Iraqi 65-bus radial distribution systems through simulation using MATLAB. Comprehensive simulation results of four different cases show that the proposed HFPSO demonstrates significant improvements over other existing algorithms in supporting voltage stability and loss reduction in distribution networks. Furthermore, comparisons have achieved to demonstrate the superiority of HFPSO algorithms over other techniques due to its ability to determine the global optimum solution by easy way and speed converge feature.

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NOMENCLATURE

NOMEN	CLAIURE		
V_R	: The voltage at receiving end bus	$x_i(t)$: Size of particles
V_{S}	: The voltage at sending end bus	$x_i(t+1)$: Updated size of the particles
V_{Rnew}	: The voltage at receiving end bus after	$V_i(t)$: Velocities of the particles
	compensated	$v_i(t+1)$: Updated velocities of the particles
θ_{new}	: Phase angle between V_{Rnew} and V_S	t	: Number of iteration
δ	: Phase angle of sending end voltage	I _{D-STATCOM}	: The injected current of D-STATCOM
α	: Phase angle of Current pass between	$S_{total \ loss}$: Total power losses
	two buses	$R_{SR} + jX_{SR}$: Impedance of branch between bus 'S' and 'R'
$V_{R,min}$: Minimum Voltage limit of bus 'R'	β_2 and β_3	: Weighting factors of objective functions β_1
$V_{R,max}$: Maximum Voltage limit of bus 'R'	$Q_{DSTATCOM(R)}$: Reactive power of D-STATCOM at bus 'R'
$P_{R(R)}$: Real power of DG at bus 'R'	P_{TL}	: Total real loss before insert DG and D-
VSIR	: Voltage stability index of node 'R'		STATCOM
AV(x)	: Average of buses voltages	$\Delta P_{TL}^{DG/DST}$: Loss Reduction Index with DG and D-
Ŵ	: Weight inertia	<i>TL</i>	STATCOM
C_{2}, C_{1}	: Acceleration coefficients	$Q_{DSTATCOM(R)}^{min}, Q_{DSTATCOM(R)}^{max}$: Minimum, maximum injected reactive power
I_L	: Current pass between two buses	CDSTATCOM(R), CDSTATCOM(R)	limit of compensated bus' R'
gbest ^{t-1}	: Global best size	$P_{R,\min(R)}, P_{R,\max(R)}$: Maximum, minimum real power limit of compensated bus 'R'



*pbest*_i : Particle best size

: Real and reactive power losses of branch between bus ${\rm 'S'}$ and ${\rm 'R'}$

1. INTRODUCTION

Nowadays, transmission and distribution power systems are facing a challenge to provide the power demands for more customers with better quality and higher reliability at a lower cost. Such growing demand increasing power transfer through lines which is limited by the thermal, voltage, and stability of lines. Consequently, when the lines are operated near to their critical limits of power angles or voltage limits, any increased demand in this system would results instability like power system oscillation and voltage collapse occurrence which may lead to generator outages and ultimately blackout [1].

Different techniques have been suggested by researchers for solving the voltage system stability issues and minimizing losses in distribution systems. Previosly, system planners are inclined to develop new lines. However, such technique is difficult to implement due to some of the economic and environmental concerns [2], [3]. So, these various restrictions on the construction of new transmission lines have persuaded the power system designers to look for some alternative solutions, so to increase the power system stability and efficiently transmit power over the transmission lines [4].

To minimize the probability of voltage collapse happening and enhance voltage stability as well as improve voltage profile, some researchers have proposed to add capacitors in an optimal location with optimal size by using different optimization techniques such as harmonic search (HS) algorithm [5], dice game optimization (DGO) [6], and modified biogeography based optimization (MBBO) algorithm [7]. However, these shunt capacitors are not capable to constantly produce a variable reactive power and exhibit some of the operational problems like resonance [2]. Such restrictions of the construction of shunt capacitors have persuaded the power system designers to look for some alternative solutions.

Recently, distribution generators (DG) are widely known as "an electric power source connected directly to the distribution network or on the customer side of the meter", that form the key part of the solutions [8]. DGs are known as small distributed generators which are consisted of renewable and nonrenewable power sources. DGs are contributed to the centralized power grids that are managed at the distribution level [9]. The integration of renewable energy sources in the conventional distribution system is becoming valuable and more attractive due to their economic and technical impacts [10]. Many researcher have adopted various types of renewable sources (fuel cell, PV, battery, biomass, wind) [11]-[14]. However, advanced devices are required to control and manage the new smart distribution grids to operate with bidirectional power flow using power electronics and energy storage units [15]. Combining the use of the distributed flexible ac-transmission system (D-FACTS) as a power electronic device with DG in the distribution networks will mitigate the problems of environmental, reliability, and stability issues [2].

The distributed static synchronous compensator (D-STATCOM) is the most important type of shunt-connected D-FACTS device, it is connected directly to low voltage distribution grids without any ancillary components which represents as an efficient shunt capacitors substitute [2]. It acts as a reactive power compensation source, harmonics reduction, power factor correction, and controlling the voltage of the distribution network [16]. Recently, the combination of DG and D-STATCOM was suggested which could compensate for the active and reactive power in smart distribution grids. The optimal location and the capacity of DGs of these sources are some of the main factors of contribution in affecting the improvement of the power quality indices such as the reduction of the distribution systems losses and maintaining the voltage profile within acceptable limits [17].

A DG with D-STATCOM was tested under different conditions to enhance the voltage stability of different load models [2], [18]. Several studies have been presented under the name of metaheuristic techniques such as "whale optimization algorithm (WOA) [17], noval light search algorithm (LSA) [2], gravitational search algorithm (GSA) [19], a combination of genetic algorithm and particle swarm optimization (GA and PSO) [20], grey wolf optimization algorithm (GWOA) [21], vortex searching algorithm [22], imperialist competitive algorithm (ICA) [8], and hybrid genetic and ant colony algorithm [16]" to determine the optimal placement problem of DG and D-STATCOM in smart power systems. Many of the above studies mentioned above have been carried out to locate the optimal location and size problems of DG and D-STATCOM devices separately or simultaneously.

Remarkably, a comprehensive study is lacking in using intelligent algorithms in exploiting the potentials of the DGs with D-STATCOM. Although, several studies have presented under the name of metaheuristic techniques. PSO and general algebraic modeling systems were proposed to solve the sizing and location of single and multiple D-STATCOM in [23]. An artificial fish swarm optimization algorithm (AFSOA) using voltage stability index (VSI) and loss sensitivity factor (LSF) was applied to deduce the size and optimal locations of DGs and D-STATCOM in [24].

Further, research on using the VSI and WOA was developed to select the proper location and best size of DG, so to enhance the voltage stability and increase the load-ability through injecting the appropriate active and reactive powers. However, the best DG place is allocating by using the VSI to find the most sensitive buses [25]. The literature clarified that the researchers are continuing to develop intelligent optimization techniques to solve global optimization problems. This paper has proposed to exploit the advantage of firefly algorithm (FA) and PSO as a fast converge optimization algorithm with good-tuning feature, so to easily achieve the global optimum solution for optimal placement and sizing of DG and D-STATCOM device to support the grid's voltage stability as well as enhance voltage profile and minimize power losses.

The motivation of this study focuses on the tabulated results which illustrate the ability of the hybrid firefly and particle swarm optimization algorithm (HFPSO) to determine the optimal placement and sizing of DG and D-STATCOM device, due to its feature to find the global optimum solution. The algorithm is based on a multi-objective HFPSO to minimize the system power losses and voltage profile enhancement as well as increasing the system stability. The verification of the proposed algorithm is achieved on the standard IEEE 33-bus and Iraqi 65-bus radial distribution systems through simulation using MATLAB.

This paper is organized as follows. Section 2 explains the system modeling, While section 3 presents the problem formulation. A hybrid algorithm combining the firefly algorithm and particle swarm optimization is introduced in section 4. In section 5, the simulation results of a distribution system under different cases with the proposed algorithm are presented. Furthermore, a performance comparison of the system is then carried out against other existing algorithms in supporting voltage stability and loss reduction in the distribution networks. Finally, section 6 gives concluding remarks on the current work.

2. SYSTEM MODELLING

2.1. D-STATCOM modelling

D-STATCOM is well-known as an efficient power electronic device control power flow [16], [26]. The basic function of the D-STATCOM is providing reactive power that depends on the reactive power exchange between the AC grid and the D-STATCOM with fast and uninterrupted power [16], [21], [27]. The injected reactive power deduce by (1).

$$Q_{D-STATCOM} = V_{rnew} \left(I_{D-STATCOM} \right)^* \tag{1}$$

Where $I_{D-STATCOM \angle}((\frac{\pi}{2}) + \theta_{new})$ is the injected current by DSTATCOM $V_{Rnew} = V_{Rnew} \angle \theta_{new}$ is the voltage of bus 'R' after correction. Figure 1(a) shows the single line diagram of two buses of a distribution system with D-STATCOM that is installed in bus 'R' Voltage of bus 'R' changes from V_R to V_{Rnew} as shown in Figure 1(b).



Figure 1. Single line diagram and the phasor diagram of two buses with D-STATCOM: (a) single line diagram of two buses with D-STATCOM [21], (b) the phasor diagram of two buses with D-STATCOM [21]

$$V_{Rnew} \angle \theta_{new} = V_S \angle \delta - (R_{SR} + jX_{SR})I_L \angle \alpha - (R_{SR} + jX_{SR})I_{D-STATCOM \angle}(\frac{n}{2}) + \theta_{new})$$
(2)

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DSTATCOM is one of the most efficient D-FACTS devices due to its features like zero resonance, less harmonic distortion, low power losses, low cost, compact size and high regulatory capability [16], [28]. D-STATCOM has been employed as multi-applications at the distribution grids, so to enhance voltage profile, minimize real power loss, improves load ability, and enhances stability [21]. However, the proper location of D-STATCOM is important to minimize the network power loss and subject to the following standard limits [29]:

Voltage limit: $V_{R,min} \leq V_R \leq V_{R,max}$

where $V_{R,min}$ is the minimum voltage limits of bus 'R' and $V_{R,max}$ is the maximum voltage limits of bus 'R'.

Injected reactive power limit: $Q_{DSTATCOM(i)}^{min} \le Q_{DSTATCOM(i)} \le Q_{DSTATCOM(i)}^{max} i = 1,2,3$, nb

Where $Q_{DSTATCOM(R)}^{min}$ is the minimum reactive power limit of the compensated bus 'R' and $Q_{DSTATCOM(R)}^{max}$ is the maximum reactive power limit of the compensated bus 'R'.

2.2. Distributed generation (DG)

DG is described as a small-scale electric power generation that has a capacity of 1 kW to 100 MW and linked adjacent to the loads. DG consists of renewable and nonrenewable sources such as micro turbines, induction generators, synchronous generators, solar photovoltaic, fuel cells, combustion gas turbines, wind turbines, and other small power generation sources. DG sources are classified into the following four types [22]:

a) DG type one: DG injects real power (P) only

- b) DG type two: DG injects both real and reactive power (P and Q)
- c) DG type three: DG injects real (P) power but absorbs reactive power (Q)
- d) DG type four: DG injects reactive power (Q) only

The main features of DGs are mitigating the greenhouse effect and using fossil fuel, improve voltage profile, energy security, reliability, stability, power quality, and reduces power losses [8], [9], [29]. Nevertheless, the optimal locations of DGs are also important to improve the system operation characteristics and subject to the following standard limits [30]:

Voltage limit: $V_{R,min} \leq V_S \leq V_{R,max}$

Injected reactive power limit: $P_{R,\min(i)} \leq P_{R(i)} \leq P_{R,\max(i)}$ i = 1,2,3, nb

where $P_{R,\min(R)}$ is the minimum real power limit of the compensated bus 'R' and $P_{R,\max(R)}$ is the maximum real power limit of the compensated bus 'R'.

3. PROBLEM FORMULATION

3.1. Load flow analysis

The direct load flow analysis is considered in this paper to find the power losses and voltage profiles of each bus developed for the radial distribution systems. The power-flow equations are written according to Kirchhoff's Current Law, a more detailed explanation of the power flow analysis can be found in [27]. The sample distribution system is shown in Figure 2. The voltage at bus 'R' is written as in (3):

$$V_{R} = V_{S} - B_{S} * (R_{SR} + jX_{SR})$$
(3)

where B_s is the bus-currents to branch-currents matrix. The total power loss of the network is calculated by summing the power losses of all the branch as shown in (4) [2]:

$$S_{total \ loss} = \sum_{s=1}^{no.branch} P_{loss}(S,R) + j \sum_{s=1}^{no.branch} Q_{loss}(S,R)$$
(4)

where the power loss in a branch between buses 'S 'and 'R' is identified by using (5) and (6) for real and reactive losses respectively.

$$P_{loss}(S,R) = \left(\frac{P_s^2 + Q_s^2}{|V_s|^2}\right) * R_{sR}$$
(5)

$$Q_{loss}(S,R) = \left(\frac{P_s^2 + Q_s^2}{|V_s|^2}\right) * X_{sR}$$
(6)



Figure 2. Single line diagram of two buses system [21]

3.2. Objective function

The multi-objective function should be modeled carefully to avoid conflicting between various single objective functions. In this paper, the objective function of the proposed algorithm is adopt a number of functions to be optimized simultaneously such as maximize voltage stability index, mitigate the power loss and enhance the bus voltage profile with a weighting factor. The weight factors are considered to determine the priority impact of every single objective function for DG/D-STATCOM interconnection. Due to the fact that, power losses have a greater effect on utilities and represent the major concern in the power system network. Therefore, it should be reduced by selected appropriate weight factors more imperative than the influence voltage stability index and voltage profile. Mathematically, the multi-objective function has as shown in (7):

$$Minimize(Fittness) = min\left(\beta_1\left(\Delta P_{TL}^{DG/DST}\right) + \beta_2\left(\frac{1}{AV(x)}\right) + \beta_3\left(\frac{1}{\Delta VSI^{DG/DST}}\right)\right)$$
(7)

where $\Delta P_{TL}^{DG/DST}$ is the ratio of the total power loss after and before adding DG/D-STATCOM in radial distribution system (RDS) which given by (8) [17].

$$\Delta P_{TL}^{DG/DST} = \frac{P_{TL}^{DG/DST}}{P_{TL}} \tag{8}$$

 $\Delta VSI^{DG/DST}$ is the ratio of the voltage stability index of weaken bus after and before adding DG/D-STATCOM in RDS which is given by (9) [2].

$$\Delta VSI^{DG/DST} = \frac{VSI_{after}^{DG/DST}}{VSI_{befor}}$$
(9)

AV(x) is the average of buses voltages which is given by (10) [15].

$$AV(x) = \left(\frac{\sum_{i=1}^{n} V_i(x)}{n}\right) \tag{10}$$

 β_1 , β_2 and β_3 are the weighting factors of the minimization power loss and maximization AV and VSI respectively which are considered as (0.7), (0.3), and (0.3) respectively.

3.3. Voltage stability index

Voltage stability is the ability of a power system to meet the increasing demand and maintain the voltage at all buses in an acceptable limit and to avoid the occurrence of the voltage collapse. The voltage

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collapse is defined as a very low voltage profile in a significant number of the system buses with a sequence of events accompanying voltage instability [1], [31].

The power system security level can be reflected by many possible indices. In this part, the VSI is applied pre-identify to identify the weak buses of radial distribution networks, in order to strengthen these buses and maintain system voltages at an acceptable level. It will add DGs and D-STATCOM in an optimal location. Then, to overcome the sup-optimal operation of the existing algorithms, the HFPSO algorithm is utilized to determine the optimal size of both DG and D-STATCOM. Moreover, the predetermining advantage of the optimal location by using VSI to minimize the search space of the optimization algorithm. The monetary value of voltage stability index can be formulated as relation in (11) [22], [24]:

$$VSI_{R} = |V_{S}|^{4} - 4(P_{R}X_{SR} - Q_{R}R_{SR})^{2} - |V_{S}|^{4}(P_{R}R_{SR} + Q_{R}X_{SR})$$
(11)

where VSI_R is the voltage stability index of node 'R' for the distribution system, which is shown in Figure 3.

4. HYBRID FIREFLY AND PARTICAL SWARM OPTIMIZATION (HFPSO)

A HFPSO is used in this study so to find the optimum DG and D-STATCOM placement and sizing. The HFPSO is introduced firstly by [32] to solve the optimization problem. The performance of the proposed hybrid optimization algorithm has significant improvements over the standard PSO and FA algorithms due to the combination of the advantages and strengths of PSO and FA, and also because it mitigates the disadvantages of these algorithms. Generally, it provides a fast convergence as PSO feature and easily achieves the global optimum solution as a good-tuning feature of FA [32]. Figure 3 shows the flowchart of the proposed hybrid of FA and PSO.



Figure 3. Flowchart of HFPSO algorithm [32]

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- To illustrate the HFPSO algorithm, the steps of the algorithm steps are described below:
- 1. Input the parameters that are used by both algorithms and initialize particles with random positions and velocities. In the considered case, the location of D-STATCOM and DG are generated in a form of vectors as algorithm particles.
- 2. Run the load flow program to calculate the fitness of each particle according to (7).
- 3. Calculate the global and personal best particles and then assigned
- 4. An improvement is done in its fitness value in the last iteration according to (12).

$$f(i,t) = \begin{cases} true, if \ fitness(particle_i^t) \le gbest^{t-1} \\ false. if \ fitness(particle_i^t) > gbest^{t-1} \end{cases}$$
(12)

5. Save the current position in a temp variable (x_{i-temp}) and calculate the new position and velocity according to (13) and (14).

$$x_i(t+1) = x_i(t) + B_{\circ}e^{-\gamma r^2 i j} (x_i(t) - gbest^{t-1}) + {}^{a \in i}$$
(13)

$$v_i(t+1) = x_i(t+1) - x_{i-temp}$$
(14)

6. Start the local search and handle particle by an imitative FA if a particle has a better or equal fitness value than the previous global best, otherwise, PSO continues its standard processes with a particle according to (15) and (16) so to handle this particle.

$$V_i(t+1) = wV_i(t) + c_1t_1(pbest_i(t) - x_i(t)) + c_2t_2(gbest_i(t) - x_i(t))$$
(15)

$$x_i(t+1) = x_i(t) + V_i(t+1)$$
(16)

- 7. Run the load flow to calculate the fitness of each particle, select the dominant one and consider it as best global fitness if it was better than the previous global fitness.
- 8. Update the best position of each particle by comparing the new position to the best global position.
- 9. If the algorithm converges, the optimization process is over. Print the optimal solution, or otherwise, go to step 4.

5. RESULTS AND DISCUSSION

To demonstrate the performance of the HFPSO method, a standard IEEE 33-bus RDS and 65-bus Iraqi RDS are used and simulated using the MATLAB. The losses and bus voltage for all the systems are calculated through the direct load flow analysis. The optimal location and sizing of DG and D-STATCOM are obtained by the proposed optimization algorithm HFPSO. To demonstrate the effectiveness of the proposed algorithm, the overall findings/results are compared with other optimization techniques such as; bacterial foraging optimization algorithm (BFOA) [18] and the PSO [10], [33], [34] for four different cases as follows: i) case 1 the system without DG and D-STATCOM, ii) case 2 the system with only D-STATCOM, iii) case 3 the system with only DG and iv) case 4 the system with multi DG and D-STATCOM.

5.1. 33-bus test system

A bus test radial distribution system is considered in this paper. To show the effectiveness of the proposed method, four different case studies have been tested. The data of the system are taken from [35]. The total load of the system is 3715 kW and 2300 KVar with the base apparent power and base voltage are 100 MVA and 12.66 kV respectively. The comparative simulation results of the proposed algorithm and other optimization techniques are shown in Table 1. Firstly, the system without DG and D-STATCOM as a base case is simulated. So, the active power losses, the minimum VSI, and the minimum voltage are 210.77 kW, 0.66734 p.u, and 0.90383 p.u, respectively as indicated in Table 1.

Then, the D-STATCOM is placed at 30th bus as the optimal location (case 2), the total power loss has been reduced to 143.6 kW and the minimum VSI is enhanced to 0.7355 p.u, while the results obtained in [18] are 144.38 kW and 0.7228 p.u respectively. In this case, the authors have taken the line data of RDS presented in [36], [37] which differs from the line data considered in this paper but the same line data considered in [27] in case placement D-STATCOM. In case 3, one DG (type one) is optimally placed in the 6th, bus with 2720 kW as an optimal size. The total power loss is reduced to 111.23 kW and the minimum

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VSI of this system is enhanced to 0.7949 p.u. Clearly, the power loss reduction and VSI enhancement, in this case, are better than other optimization methods as illustrates in Table 1. Finally, in case 4, three DG and three D-STATCOM are placed in the system at optimal locations to reduce the power losses and to improve the minimum VSI of this system. The obtained results are presented in Table 1. The total power loss is reduced to 13.8 kW and the minimum VSI is enhanced to 0.9415 p.u. It is noticed that the results in case 4 are better than the results of other algorithms. Obviously, the HFPSO gives a good reduction in losses and the voltage profile of the system has been improved noticeably compared to other algorithms. A comparison of the voltage profile, stability voltage index and the total power losses for the four different cases are shown in Figure 4(a), 4(b), and 4(c) respectively.

Table 1. The comparative simulation results							
	Variable	HFPSO	BFOA [18]	PSO [10], [33], [34]			
Case 1	Ploss (kW)	210.77	210.98	210.99			
	VSImin (p.u.)	0.66734	0.6610	0.6671			
	Vmin (p.u.)	0.90383	0.9037	0.9038			
Case 2	Size in kVAr (location)	1300 (30)	1102.7 (30)	1233 (7)			
	Ploss (kW)	143.6	144.38	153			
	VSImin (p.u.)	0.7355	0.7228	0.726			
	Vmin (p.u.)	0.9261		0.922			
Case 3	Size in kW (location)	2720(6)	2200 (6)	2895.1 (7)			
	Ploss (kW)	111.23	113.14	114.89			
	VSImin (p.u.)	0.7949	0.7640				
	Vmin (p.u.)	0.9442	0.9368	0.9501			
Case 4	Size in kVAr (location)	390 (12)	400 (12)	603.4 (8)			
		650 (24)	350 (25)	466.3 (22)			
		840 (30)	850 (30)	856.7 (30)			
	Size in kW (location)	880 (12)	850 (12)	1015.4 (9)			
		870 (24)	750 (25)	351.4 (24)			
		1030 (30)	860 (30)	8445 (30)			
	Ploss (kW)	13.8	15.07	27.3993			
	VSImin (p.u.)	0.9415	0.9376				
	Vmin (p.u.)	0.985	0.9862	0.975			



Figure 4. Comparison of results for the four different cases: (a) comparison of voltage profiles for different cases in 33-bus system, (b) comparison of VSI for different cases in 33-bus system, and (c) comparison of line losses for different cases in 33-bus system

5.2. The 65-bus system numerical results

The Iraqi real 65-bus radial distribution system is simulated as a second test system under four different case studies. Figure 5 shows the system's configuration. The system data is given in Table 2 and the results are presented in Table 3. The total load of this RDS is 5669.1 kW and 3560.6 KVar with base apparent power and base voltage are 100 MVA and 11 kV respectively. The active power losses, the minimum VSI, and the minimum voltage of the base case are 446.2 kW, 0.645 p.u, and 0.8962 p.u, respectively.



Figure 5. Iraqi real 65-bus configuration

Table 2. 65 bus system data											
	From	То	R (p.u)	P_L	Q_L		То	R (p.u)	X (p.u)	P_L (MW)	Q_L (MVAr)
1	1	2	0.216363	(MW)	(MVAr)	33	34	0.006175	0.007538	0.1700	0.1054
2	2	3	0.18478	0.1063	0.0659	34	35	0.045125	0.055081	0.1063	0.0659
3	3	4	0.159363	0.1063	0.0659	35	36	0.032063	0.039137	0.1063	0.0659
4	4	5	0.06318	0.0	0.000	36	37	0.030875	0.037687	0.0	0.000
5	4	6	0.025650	0.1700	0.1054	37	38	0.046550	0.056820	0.1063	0.0659
6	6	7	0.011400	0	0	38	39	0.015200	0.018554	0.0	0.0
7	6	8	0.077663	0.1063	0.0659	39	40	0.056763	0.069286	0.1700	0.1054
8	8	9	0.004750	0.0	0.00	40	41	0.018763	0.022902	0.0	0.0
9	8	10	0.073625	0.1063	0.0659	41	42	0.021138	0.025801	0.1063	0.0659
10	10	11	0.022325	0.0	0.000	42	43	0.045600	0.055661	0.1700	0.1054
11	10	12	0.024938	0.1063	0.0659	43	44	0.022088	0.026961	0.1063	0.0659
12	12	13	0.066025	0.0	0.000	44	45	0.026363	0.032179	0.1700	0.1054
13	12	14	0.032300	0.1700	0.1054	45	46	0.037525	0.045804	0.0	0.00
14	14	15	0.030875	0.1700	0.1054	46	47	0.055813	0.068127	0.1063	0.0659
15	15	16	0.031588	0.0	0.0	47	48	0.007600	0.009277	0.1063	0.0659
16	15	17	0.089538	0.1700	0.1054	48	49	0.021375	0.026091	0.0	0.000
17	17	18	0.017100	0.0	0.0	49	50	0.009975	0.012176	0.1063	0.0659
18	17	19	0.014725	0.1063	0.0659	50	51	0.029688	0.036238	0.1700	0.1054
19	19	20	0.015675	0.0	0.000	51	52	0.006413	0.007827	0.0	0.000
20	19	21	0.095238	0.1063	0.0659	52	53	0.081225	0.099146	0.1700	0.1054
21	21	22	0.121838	0.0	0.0	53	54	0.016150	0.019713	0.0	0.000
22	21	23	0.113050	0.1700	0.1054	54	55	0.018525	0.022612	0.1700	0.1054
23	23	24	0.016388	0.0	0.0	55	56	0.018763	0.022902	0.1700	0.1054
24	23	25	0.011400	0.1700	0.1054	56	57	0.002850	0.003479	0.1063	0.0659
25	25	26	0.001663	0.0	0.0	57	58	0.013538	0.016524	0.1063	0.0659
26	25	27	0.027550	0.1063	0.0659	58	59	0.012588	0.015365	0.0	0.00
27	27	28	0.008550	0.0	0.0	59	60	0.009500	0.011596	0.1063	0.0659
28	28	29	0.011638	0.1063	0.0659	60	61	0.050113	0.061169	0.1700	0.1054
29	29	30	0.020900	0.1700	0.1054	61	62	0.026125	0.031889	0.1063	0.0659
30	27	31	0.015675	0.1700	0.1054	62	63	0.022800	0.027830	0.0	0.000
31	31	32	0.021613	0.0	0.0	63	64	0.021138	0.025801	0.1700	0.1054
32	31	33	0.069113	0.1700	0.1054	64	65	0.024938	0.030439	0.1700	0.1054

Table 2. 65 bus system data

It is depicted from Table 3 the total power loss is reduced to 300.3 kW and the minimum VSI is enhanced to 0.7941 p.u after D-STATCOM is placed at the 33th bus as the optimal location in case 2. While

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in case 3, one DG (type one) is optimally placed in the 33th bus with 5020 kW as the optimal size. The total power loss is reduced to 122 kW and the minimum VSI of this system is enhanced to 0.8367 p.u. In case 4, both three DG and one D-STATCOM are installed at optimal locations to reduce the power losses and to improve the minimum VSI of this system. The obtained results are presented in Table 3. However, the total power loss is reduced to 12.2 kW and the minimum VSI is enhanced to 0.9707 p.u after a multi DG and D-STATCOM are placed at the optimal locations. A comparison of the voltage profile, stability voltage index, and the total power losses for the four different cases are shown in Figure 6(a), 6(b), and 6(c) respectively.

Table 3. 65-bus numerical results							
	Case 1	Case 2	Case 3	Case 4			
Size in MVAr (location)		3.34 (33)		2.77 (33)			
Size in MW (location)			5.02 (33)	3.96 (34)			
				0.39 (39)			
				1.62 (3)			
Ploss (kw)	446.2	300.3	122	12.2			
Qloss (kvar)	544.6	367	148.9	14.9			
VSImin (p.u.)	0.645	0.7941	0.8367	0.9707			
Vmin (p.u.)	0.8962	0.9440	0.9564	0.9926			



Figure 6. Comparison of results losses for the four different cases: (a) comparison of voltage profiles for different cases in Iraqi 65-bus system, (b) comparison of VSI for different cases in Iraqi 65-bus system, and (c) comparison of line losses for different cases in Iraqi 65-bus system

6. CONCLUSION

In this paper, a new optimization technique based on HFPSO has been proposed to enhance the system stability of smart distribution grids. The main advantage of the proposed algorithm is to combine the advantages and strengths of PSO and FA and to mitigate the disadvantages of these algorithms. HFPSO is employed to solve a multi-objective function including voltage stability enhancement and minimizing the

total power loss by finding the optimal locations and sizes of DG and D-STATCOM in the power distribution system. Actually, The effectiveness of the proposed algorithm has been tested on two power systems. Besides, the overall results were, compared with some other optimization techniques such as BFOA and PSO under four different cases. Comprehensive simulation results show that the proposed HFPSO algorithm achieves significant improvements compared to other optimization algorithms in supporting voltage stability and in minimizing the power losses in distribution networks. Generally, HFPSO provides a fast convergence as PSO feature and easily achieves the global optimum solution as a good-tuning feature of the firefly algorithm. Furthermore, it could be concluded that the HFPSO would simplify the use, as an intelligent real-time tool with any large distribution system.

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