Analysis and simulation of even-level quasi-Z-source inverter

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Article Info

ABSTRACT

Article history:

Received Feb 19, 2021 Revised Mar 16, 2022 Accepted Mar 29, 2022

Keywords:

Duty cycle Harmonic spectra Multilevel inverter Quasi Z-source Seven-level This research proposes a seven-level inverter with quasi-Z-source boost converters. The proposed topology employs a packed U-cell asymmetrical type multilevel inverter along with front-end quasi-Z-source networks. The quasi networks provide high gain compared to a conventional boost converter. This topology is the most suitable for photovoltaic multi-string applications. The proposed topology has the potential to supply both the alternating current (AC) and direct current (DC) type load. The inverter structure has a lower number of active switches which helps in the reduction of losses and improvement in efficiency. In this paper, the operation principle of a quasi-network and inverter circuit are explained in detail. In addition, the simulation results for various modulation indices are presented. In the MATLAB/Simulink environment, the architecture is proposed by using gated sinusoidal "Pulse width modulation".

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1. INTRODUCTION

Latest developments have seen considerable rise in the utilization of Z-sources based converters in possible solutions such as environmentally ecofriendly fuel cell-based generations/photovoltaic (PV) to fulfil expanding energy demands, flexible alternating current (AC) transmission systems (FACTs), energy storage, electric and electric vehicles as well as in wind energy conversions [1]. In comparison by the direct current (DC-DC) two-stage conversions, the effectiveness of single-stage conversion improves as a result of this. The Z-source inverters (ZSI) alleviate the failure of outdated current source inverters and voltage supply by using a network of two inductors and two condensers in the shape of a Z [2]. This impedance network introduction eliminates inverters failure due to the lack of dead band in the absence of the leg switches and thus reduces the waveform distance. By changing the duty cycle D0, the output voltage is controlled phase switches or all phases to be activated over the cycle duration.

A review of various strategies is presented [3]. To achieve the appropriate output tension, traditional pulse-width modulation (PWM) methods are modified to include a zero-status shoot-through without changing the active circumstances. The optimal positioning of the screw is, however, obligatory as it takes a prominent place in the evaluation of the current ripple, number of switch switches, minimization of switching loss and softness. In this aspect, a new control system [4] is investigated, which uses zero voltage switching (ZVS) to effectively reduce commutations for simple control and enhanced efficiency. A better control system is being investigated in the same area [5]. Both legs are used to shoot, reducing the current stress

between the switches. The higher as well as lower frequencies of the switch's fs and 2fs are different, which increases the loss. The technique is modified in this paper to allow all switches to operate at the same frequency (s) to reduce the loss of switching. In comparison to ZSIs, the benefits of constant input current, reduced capacitor voltage stress, and smaller C2 make quasi Zsource inverters (qZSI) highly attractive for renewable applications. Multi-level inverters (MLIs) for low-power applications have recently gained the benefits of low dv/dt, minimal button stress, improved voltage and current profiles, and reduced filter size [6]. H-bridges in cascade (CHB), neutrally point clamped (NPC), and flying condensers are three prominent topologies utilized in industrial applications (FCs). CHB is the most suitable of these due to its adaptability, lack of clamping diodes, and lack of FC-voltage balance issues. Switch counts, condenser reduction, diodes, condenser equilibrium, simplicity of control, and the quantity of DC sources have all been studied in MLIs [7]. Although MLIs provide a number of advantages, one of the most significant drawbacks is the low output voltage gain. In order to achieve improved voltage control and output quality, MLIs must be properly upgraded with appropriate power conditioners [8]–[14]. The power conditioner for MLI integration is a Z source-based converter.

The recent growth in the adoption of Z-Source converters has revolutionized renewable energy system including power electronic application, hybrid cars, uninterruptable power supplies, and distributed energy [15]. Inverter capitalizes on the problems that traditional current source and voltage source inverters [16]. This reduces wave form distortions and improves dependability. It reduces DC power consumption when combined with a buck-boost circuit, resulting in a more efficient single-stage. In order to maximize the amplitude of the shoot-through voltage, the service series is boosted by the output voltage. The beam-through can be obtained by turning on the switches for DT. The different methods for shoot-through control are described in the literature [17], [18]. In general, the Z-source converters are more common with conversions from DC to alternating current (AC) as well as AC to DC. Because of the numerous Z-sources topologies [19]–[22], most systems use quasi-Z inverters, which minimize the capacitor size, thus offering continuous input current, as well as having DC input, but are not common-rail devices.

In contrast, a multi-level inverter (MLI) delivers better voltage and current with lower total harmonics distortion (THD), which reduces switching losses and increases efficiency. A number of more advanced MLI topologies, including neutral point (NP) capacitor, switch count (SC) capacitor, and the cascaded chronic myeloid leukemia blast crisis (CML BC), have been employed in order to resolve the issues of switching, capacitor voltage balancing, and the difficulty of managing complexity [23]. For another important effort, MLI is also being made to comply with lower voltage distributed energy sources, which means the biggest issue with MLI is low output voltage gain, however [24], [25].

Higher voltage gains and seven-level AC output with fewer switching devices, fewer DC power supply, as well as minimum off state voltages pressure acrossed the converting device are all advantages of the proposed converter. The rest of the manuscript is laid out: under second subpart of paper explain proposed approach of inverter and operating modes, under third subpart of paper explains the modulation principle used to generate the required output voltage waveform, under fourth subpart of paper shows how the new converter design which proposed by author is validated using simulation results for various modulation indices, and section 5 finally concludes all pros and corn of this research.

2. PROPOSED INVERTER

Figure 1 represents the developed quasi of Z-source single phase seven levels created MLI using a packed u-cell structure. The z-source network is formed by the elements called inductors, diodes capacitors and an active switch. The inverter circuit consists of 6 active switching devices with bi-directional conducting capability. Impact of anti-parallel diodes, the switching device has bi-directional leading capability but only block voltages in uni-directional. In the suggested topology, three different DC source can be generated after batteries bank, PV system, or rectifiers circuits. The major contribution of this paper is the cascaded connection of packed U-cell (PUC) inverter to the quasi-Z-source. This cascaded connection gives the higher output voltage, better performance and improved harmonic profile which is shown with the simulation results.

Figures 2(a) and 2(b) represent the switching conditions through negative along with positive zeroes crossings of the output voltage. $V0=0^+$ is the positive zero-crossing through the output voltage. $V0=0^-$ is the negative zero-crossing at output voltage. To keep the temperature escalation in entire switches at the same level, both switching states are used equally.

Figure 3 shows the recommended converter, which operates to create a positive level voltage transversely the output terminal. Figure 3(a) generated V0=V1, and the power semiconductor devices insulated gate bipolar transistors (IGBTs) S5, S7, and S10 operate in this manner. As illustrated in, the

IGBTs S6, S7, and S9 operate in this manner Figure 3(b). The peak voltage of V0=V1+V2 is shown in Figure 3(c), and the IGBTs S5, S7, and S9 conducted in these operating modes.



Figure 1. Proposed Z-source inverter the schematic circuit diagram



Figure 2. Zero switching states: (a) $V_0=0^+$ and (b) $V_0=0^-$

Figure 4 depicts the converter's employed mode for producing negative output voltage levels. V0=-V1 is generated in Figure 4(a), and the IGBTs S6, S8, and S9 turn on in this operating mode. The output voltage V0=-V2 is shown in Figure 4(b), and the IGBTs S5, S8, and S10 turn on during this time. The output voltage VL=-(V1+V2) is shown in Figure 4(c), and the IGBTs S6, S8, and S10 are turned on at this time.



Figure 3. Positive switching states (a) $V_0=V_1$, (b) $V_0=V_2$, and (c) $V_0=V_1+V_2$



Figure 4. Negative switching states (a) $V_{\rm L}$ =- $V_{\rm dc}/2$, (b) VL=-3 Vdc/2, and (c) VL=-2 Vdc

3. METHOD

3.1. Modulation technique

Table 1 shows the off and on conditions of the switching devices in the planned convertors on various output voltage value to help understand the switching states. The numerals 1 and 0 in Table 1 represent the off and on state of the IGBT in the Figure 1 based results. Lower switching frequencies appear to be used by switches S7 and S8, resulting in lower switching losses. In the designed architecture, the modulation technique working for generation of gate pulse to the IGBT is depicted in Figure 5. A sine wave is placed over six trilateral waveforms. The carrier waveform is known by way of the triangle waves, whereas the reference waveform is known as the sinusoidal waves shown configuration constraints in Table 2. Respectively carrier waveform interrelates with the reference waveform at certain intermissions, as specified by the digits 1, 2, 3, 1', 2', and 3'. As a result of these connections among the carrier waves and reference, the Produced pulsations are N1-N3 and P1-P3. These pulsations are successfully used in logical gate circuit uses to produce the mandatory output voltages of seven-level. The modulation index (M.I.) regulates the amount of output stages that is explained using (1).

$$M.I. = \frac{V_{0peak}}{3 \times V_{dc}} \tag{1}$$

Table 1. Switching sequences of inverter										
Output Voltage Level (V_0)	S 1	S2	S3	S4	S5	S6	S 7	S 8	S9	S10
$V_1 + V_2$	0	0	0	0	1	0	1	0	1	0
V_2	0	0	0	0	0	1	1	0	1	0
V_1	0	0	0	0	1	0	1	0	0	1
0+	0	0	0	0	1	0	0	1	1	0
0-	0	0	0	0	0	1	1	0	0	1
$-V_1$	0	0	0	0	0	1	0	1	1	0
$-V_2$	0	0	0	0	1	0	0	1	0	1
(V + V)	0	0	0	0	0	1	Δ	1	Δ	1





rable 2. Configuration constraints						
Parameters	Values					
"V _{dc} (V)"	240 V					
"Poutput (W)"	730					
$V_0(V)$	230					
"I ₀ (A)"	3.5					
"Switching frequency (f_{sw}) "	4 kHz					
"Fundamental frequency (f_m) "	50 Hz					

Table 2. Configuration constraints

4. RESULTS AND DISCUSSION

To demonstrate its performance, the proposed configuration is evaluated in a MATLAB simulation. The simulation settings are adjusted to 230 V and 50 Hz for a single-phase output voltage. Figure 6(a) shows that currents waveforms and the inverter output voltage intended for an M.I. of 0.6 and 0.9 respectively. Figure 6(a) depicts a corresponding current and the 9-level output voltage waveforms. Figure 6(b) depicts a seven-level output voltage waveforms and the comparable load currents. Lowering M.I. lowers the output voltage's peak value, which is self-evident (V0 peak). For various values of M.I., the fast Fourier transform spectrum of the inverter's output voltages is revealed in Figure 7(a) as well as Figure 7(b). V0 peak is seen to be 361 V, at the condition of the inverter is modulation value is 0.9 and the THD is 16.6%. As demonstrated in, a M.I. is invertional proportional of THD as a result of a decreasing in the amount of output voltage level.

Figures 8(a) and 8(b) represented the harmonic spectrum of the output current waveform. The rate of I0 peak is 6.4 A at an inflection of 0.9, and the THD is about 0.5%. The I0 peak value reduces in the same way as the voltage decreases when the MI decreases. The THD is coarsely 0.6%, besides the I0 peak value is 5 A.



Figure 6. MATLAB based results at (a) MI=0.9 and (b) MI=0.6



Figure 7. Fast Fourier transform analysis of (a) V₀ for (MI=0.9) and (b) V₀ for (MI=0.6)



Figure 8. Fast Fourier transform analysis of (a) I₀ for (MI=0.9) and (b) I₀ for (MI=0.6)

5. CONCLUSION

Presented research work gives a comprehensive investigation of the seven-level operational methods of the proposed quasi-Z-sources constructed multi-level inverter (MLI) with a concentrated constituent amount. The proposed network topology is a two-stage circuit that provides independent control of the output variables. The modulation technique for generating inverter switch firing pulses has been refined. The simulation results are shown for a variety of M.I. values and power ratings. The output parameters were subjected to a fast fourier transform (FFT) analysis, and the percent THD of the current waveforms was found to be within the IEEE 1547 grid standard's restrictions.

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