

Constrained discrete model predictive control of a greenhouse system temperature

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Article Info

Article history:

Received Mar 9, 2020

Revised Jul 27, 2020

Accepted Aug 7, 2020

Keywords:

Constraints

Greenhouse

Linear system

Model predictive control

Temperature control

Optimization

Yalmip

ABSTRACT

In this paper, a constrained discrete model predictive control (CDMPC) strategy for a greenhouse inside temperature is presented. To describe the dynamics of our system's inside temperature, an experimental greenhouse prototype is engaged. For the mathematical modeling, a state space form which fits properly the acquired data of the greenhouse temperature dynamics is identified using the subspace system identification (N4sid) algorithm. The obtained model is used in order to develop the CDMPC strategy which role is to select the best control moves based on an optimization procedure under the constraints on the control notion. For efficient evaluation of the proposed control approach MATLAB/Simulink and Yalmip optimization toolbox are used for algorithm and blocks implementation. The simulation results confirm the accuracy of the controller that guarantees both the control and the reference tracking objectives.

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1. INTRODUCTION

Nowadays agricultural green houses industry is considered as one of the most important and growing segment of all agri-food domains. In fact seeking new varieties, sustainable, high-performing and affordable production methods to create powerful yields and higher quality of the plants, and to reduce the industry's impact on the environment have always had a strongly held value in agricultural economics and innovation of all time. The control of the climatic environment indoor greenhouses has gained considerable attention in the past few years [1, 2]. The main reasons for this increasing interest are related to different factors one to be cited agronomic and financial ones.

As a matter of fact, a large number of methods regarding the control of the climatic conditions under greenhouses has been developed and elaborated, hence several teams in applied research have experienced this techniques to fathom and to enhance green houses control outstanding, among them: the fuzzy control [3, 4], predictive control [5, 6], in addition to neuronal networks control [7, 8], optimal control [9] and many other techniques that have emerged in many literature articles. In the control theory, model predictive control has

emerged many research and development areas. Thanks to its advantages and roles, this control technique has been present in various industrial process automation [10–12], among of them the control of greenhouses' inside climate, one can refer to [13, 14] and reference therein.

Furthermore, Model predictive control (MPC) is a widely used method for a large variety of systems, its simplicity of use makes it applicable for single, multivariable, linear and nonlinear systems and where the notion of nonlinearities and constraints incorporation, such as limitations on the sign and amplitude of the states and controls; regarding the control law synthesis; is always involved. In this sense, designing controllers that maintain the system's performances regarding these constraints is a topic of continuing evolution, hence several are the MPC approaches that have been suggested and studied by researchers. For instance, we can refer to [15–21] and many others as well. The problem addressed in our framework, is related to regulation task of inside greenhouse temperature, among various modern control strategies, model based predictive control is chosen as a technique to overcome this problem.

The main purpose of the proposed control theory, is to calculate an objective and quadratic cost function over a finite horizon of the current state and control trajectory, while satisfying constraints on the control. To do so, an algorithm developed using Yalmip optimization toolbox [22] in the form of an object oriented code is used simultaneously with an interpreted MATLAB function block that will hold this latest for simulation purposes under Simulink. The control law synthesis using a new toolbox as Yalmip together with Simulink models and blocks allow in one hand respecting the main CDMPC strategy and in another hand minimizing overhead and unneeded calculations by using an optimizer object, thing that was not treated before, regarding our inside climate parameter control case of study.

It's worth mentioning to point that the particular novelties of the present paper could be summarized as follows:

- Using an optimal method as MPC to automatically control inside climatic parameters for industrial greenhouse as a complex system.
- The utility of MPC as a perfect control approach that allows direct incorporation of constraints to an objective function.
- Providing the control activities using an optimizer with Yalmip optimization toolbox that incorporates an efficient technique which solves the problem as fast as possible.

The remaining of the paper is structured as follows, The second section steps through the greenhouse model identification and a reminder of CDMPC purposes and controller strategy, including optimization aims, parameters choice and constraints notions, in addition to the main principles of the algorithm used in our work. In the third section simulation results and discussion related to the CDMPC design strategy and synthesis will be provided. Conclusions and some of our future perspectives will be presented at the last section of this paper.

2. ENGAGED MATERIALS AND METHODS

2.1. Description of the greenhouse system prototype

As depicted in Figure 1 the experimental greenhouse engaged as support in this framework is a prototype installed at the Laboratory of Electronics, Automatics and Biotechnology (LEAB), Faculty of Sciences, Meknes, Morocco. This system is a polyethylene single wall construction, equipped with four sensors that provide indoor and outdoor measurements of temperature and relative humidity. More consicely, a LM35DZ and a HIH-4000-001 Honeywell sensors are installed to provide respectively the indoor/outdoor temperature and relative humidity measurements. Besides, several actuators are present as well; a heating system and a thermostatically variable speed fan; equipied the greenhouse to insure the appropriate climate for the system' s inside parameters.

For control and data acquisition aims, the mentionned sensors and actuators are connected to a control and acquisition cards attached to a personal computer [23]. Firstly, the acquisition of the actuators different orders and data are ensured by an acquisition data card NI-PCI6024E from Advantech family. In this regard signals conditionning, protection and power cards dedicated to the sensors and the hole system protection, are also installed. Secondly, the control and supervision tasks; that manage the system and provide a historical database of both measured indoor and outdoor climate variables; are created respectively under MATLAB/Simulink and Labview as software programs.

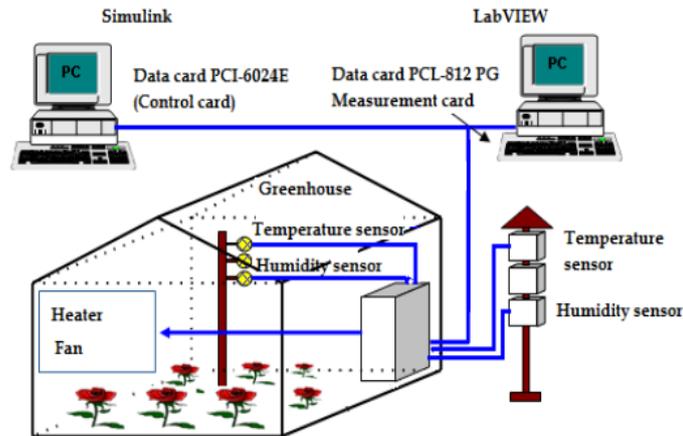


Figure 1. Experimental greenhouse system

2.2. Mathematical model for controller design

In the present section, a mathematical model of the inside temperature under greenhouse has been presented. Regarding this, a state space model describing; the greenhouse inside temperature dynamic response to the Fan as first actuator and then to the heater as second actuator; is proposed. The model used will enable us to modify the behavior of the plant to suit our needs in term of reference temperature tracking and control performances. In order to develop the controller synthesis and behavior, the plant model has to be obtained. For this aim, the system model is estimated using experimental collected data and the N4sid algorithm to identify the plant in discrete time state space model that describes the behavior of the inside temperature of the greenhouse.

For linear subspace identification, systems and models of the form (1), are generally used.

$$\begin{cases} x_{k+1} = Ax_k + Bu_k + Kw_k \\ y_k = Cx_k + Du_k + v_k \end{cases} \quad (1)$$

Where x_k , u_k , y_k , w_k and v_k are respectively the state, input, output, process and the output measurement noises vectors and A , B , C , D , K are respectively the state, input, output and noise matrix to be estimated.

Based on (1) and for simplicity, the class of systems to be considered is linear discrete-time systems with external disturbances of the form.

$$\begin{cases} x_{k+1} = Ax_k + Bu_k + Kw_k \\ y_k = Cx_k \end{cases} \quad (2)$$

An advantage of the N4sid method is that it uses a prediction error based on a the Best Fit (BF) displayed percentage related to the output reproduced by the model [24], the formula used in this regard is:

$$Bestfit = \left(1 - \frac{|y - \hat{y}|}{y - \bar{y}}\right) \times 100 \quad (3)$$

where y , \hat{y} and \bar{y} are respectively the measured, the predicted model and the mean of the output y .

The proposed control strategy has been suggested for a greenhouse system case of study, where the main task involves internal temperature regulation using heating and ventilation. To illustrate the dynamical behavior of our system depicted in Figure 1, and for the control strategy purposes mentioned above, the discrete time state space model is further used, where the behaviour of the temperature under the greenhouse process is described by the two state-space formulations as detailed in the next subsections.

2.2.1. Internal temperature responses to actuators

The main goal in this section is to use the collected data in order to have linear models that will be used as basics for the mathematical identification as follows.

- Temperature response to fan

In the present part, we describe the evolution of the internal temperature by exciting the system with a step input of 1.6 Volts that was sent to the fan in order to decrease the air temperature under greenhouse until reaching a steady state. Experimental collected data and the N4sid algorithm under Matlab are engaged to develop the corresponding discrete time state space model matrix for 5 seconds as sample time. The evolution of the measured and simulated inside temperature using the N4sid algorithm is shown in Figure 2:

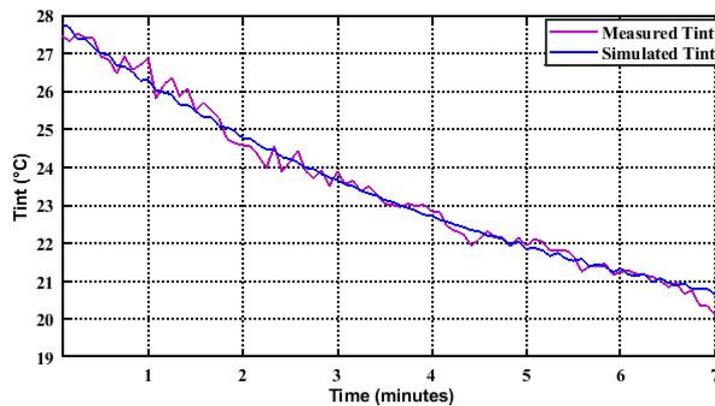


Figure 2. Comparison of simulated and experimental tint step response to a fan

Here the inside temperature reaches its 20.6°C, where the initial value is 27.9°C. The model best fit is about 90.34%, hence the state space model identification describes 90.34% of the behavior of the process output. We can conclude that the simulated and experimental results closely match each other with a good accuracy.

For the controller utilities, the identified model must be converted to a discrete-time system, considering above state space model (2), a discrete linear time invariant system with 3 states, was obtained as follows:

$$A_f = \begin{bmatrix} 0.9843 & -0.0125 & 0.0100 \\ 0.0294 & -0.8090 & 0.6507 \\ 0.0032 & -0.6512 & -0.6447 \end{bmatrix}$$

$$B_f = [-0.0127 \quad -3.3205 \quad 4.2182]^T$$

$$C_f = [23.2656 \quad 1.0200 \quad -0.1778]$$

$$D_f = 0$$

$$K_f = [-0.0152 \quad -0.0580 \quad 0.0437]^T$$

Under the initial state:

$$x_{f0} = [-1.2128 \quad -0.3375 \quad -1.4972]^T$$

And the open-loop eigen values:

$$\sigma(A_f) = \{0.9840, -0.7267 \pm 0.6457i\}$$

The index 'f' sticks to above matrix refers to the fan as input actuator engaged in the system state space identification.

- Internal temperature response to heater

The same as in the fan case, the evolution of indoor temperature was also described by exciting the system with a step input of 2.6 Volts that was sent to the heater, hence the air temperature under greenhouse was increased reaching by that a steady state for the same sample time, which is 5 seconds. In this case, the evolution of the measured and simulated inside temperature using the N4sid algorithm is shown in Figure 3 :

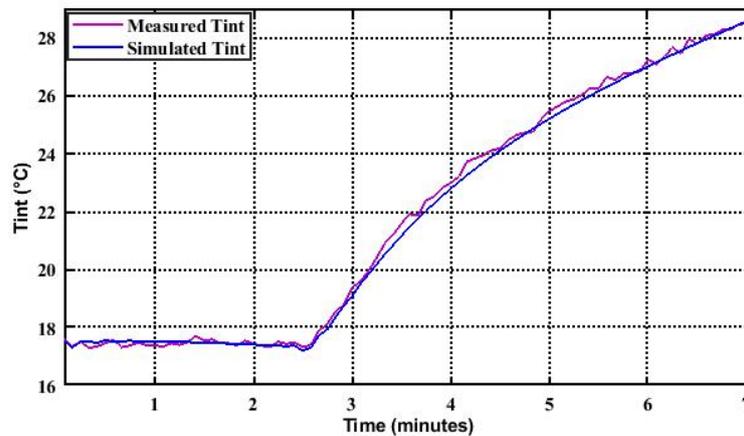


Figure 3. Comparison between simulated and experimental tint step response to a heater

As shown, the inside temperature reaches its 28.5°C, where the initial value is 17.6°C. The model best fit this time is 95.5%.

The identified discrete-time system model, with 5 states, was presented as follows:

$$A_h = \begin{bmatrix} 1.0061 & -0.0053 & 0.0034 & 0.0007 & 0.0007 \\ 0.0176 & 0.9845 & 0.1607 & -0.0906 & -0.0168 \\ 0.0003 & -0.1011 & 0.4634 & -0.8349 & -0.1410 \\ 0.0273 & 0.0027 & -0.0009 & -0.2943 & 0.6977 \\ -0.0601 & 0.0194 & -0.2084 & -0.3336 & -0.7432 \end{bmatrix}$$

$$B_h = [0.0000 \quad 0.0263 \quad 0.0247 \quad 0.1198 \quad 0.0384]^T$$

$$C_h = [184.9508 \quad 0.8560 \quad -0.4289 \quad -0.2221 \quad 0.2199]$$

$$D_h = 0$$

$$K_h = [0.0036 \quad -0.0933 \quad 0.1762 \quad 0.1326 \quad 0.0519]^T$$

Under the initial state:

$$x_{h0} = [0.0944 \quad -0.1066 \quad -0.5345 \quad 0.2705 \quad 0.2285]^T$$

And the open-loop eigen values:

$$\sigma(A_h) = \{0.9406, 0.6172, 0.9936, -0.5727 \pm 0.5166i\}$$

The index 'h' refers this time to the heater as input actuator used in the system state space identification as well.

Both identified state space models, indicate that the system is stable, controllable and observable.

2.3. Controller design

2.3.1. MPC and optimization problem brief insight

In general, MPC controller is a strategy based on an iterative, finite horizon (constrained) optimization of a plant model [25]. An actual or estimated State x_k is obtained at each discrete sampling time (k) with the sampled plant model and a cost function is calculated to obtain the performances of the controller in the future based on the current plant state x_k and a serie of future inputs u_k .

The cost function is primordial in predictive controller, that allows us to calculate the best series of control inputs u_k , which results in a minimal cost in order to keep the output as close as possible to the reference. In control field, having a cost that describes how good our control will be in the future: starting from the next step up to the end of the horizon, is the most important task to take into account. For this aim, a function of the form (4), can be expressed:

$$J = f(x_k, u_k) \quad (4)$$

Where x_k is current state and u_k is the control input.

More precisely, the cost function regarding the argument u_k has to be minimized in order to get an optimal inputs sequence u_k^* , which can be written as follows:

$$u_k^* = \arg \min_u J(x_k, u_k) \quad (5)$$

Which defines an optimal control problem.

The quadratic programming (QP) notion, results in Linear quadratic control, which is related to algorithms based on optimal control as clarified above. The integration of the cost function (5), is chosen to be quadratically dependent on the control input and the state or output response.

In this sense, linear quadratic regulators (LQR) are a special case of the generic linear quadratic control problem, where a gain matrix K that minimizes an optimization proplem cost function of the form (6), is calculated.

$$\underset{u}{\text{minimize}} \quad J = \sum_{k=1}^N x_k' Q x_k + u_k' R u_k \quad (6)$$

where N is the prediction horizon, Q and R represent positive-semi definite penalty matrices respectively. For more details about (LQR), the reader can refer to [26] and reference therein.

- Quadratic programming parameters

The linear MPC optimization results in quadratic programming (QP) problem. Hence, various are the methods used in this regard such as active-set methods and interior-point methods to solve the problem. Once an optimal solution, i.e., a control input sequence along prediction horizon is numerically obtained, we only use the first element of the sequence as an actual control input.

In addition to MPC parameters, the performance of the predictive controller depends more and more on two other important parameters to be set. These latests are the penalization matrices Q and R . Concoidering (6), it is remarquabale that both ; the state penalization matrix Q , the input penalization matrix R contribution; will affect the desired cost function.

- MPC and constraints contribution

The real meaning of a CMPC lies in computing optimal control actions for systems with constraints contribution [27]. The constraints notion regarding MPC cotroller, could simply be defined as a set of limits on the systems input variables, output or possibly states, which is presented as follows:

$$\underline{u} \leq u_k \leq \bar{u} \quad (7)$$

$$\underline{x} \leq x_k \leq \bar{x} \quad (8)$$

One can be aware that these constraints have to be reexpressed and evaluated by the mean of quadratic programming (QP) algorithms and suitable solvers. The MPC controller logic and algorithm will remain the same in the presence of constraints, the only thing to be changeable is the method of the optimization. The advantage in this case is that procedure has to be performed at every sampling instant, hence, inputs are computed in a way that they are optimal as possible and guaranteeing closed-loop stability notion. For this aim, the cost function optimization task (6) is rewritten as follows:

$$\begin{aligned} \underset{u_k}{\text{minimize}} \quad & J = \sum_{k=1}^N x_k' Q x_k + u_k' R u_k \\ \text{subject to} \quad & u_{min} \leq u_k \leq u_{max} \end{aligned} \quad (9)$$

The suffix “min” and “max” are the lower and upper constraint input bounds.

2.3.2. The adopted controller

In the present section, the CDMPC formulation for greenhouse temperature control is presented as a quadratic programming (QP) problem that is solved at each sample time. The conceptual model of the control strategy is depicted in Figure 4.

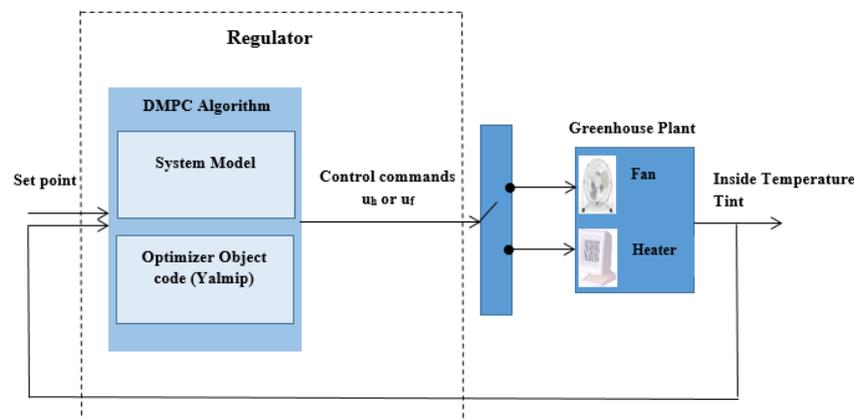


Figure 4. General conceptual model of the proposed control strategy

The constraint on the control notion regarding the system dynamics is brought into the cost function for MPC formulations. Since, the considered system dynamics are linear, the temperature control algorithm would typically involve a linear program (LP) engaging a linear cost function that will be solved using (QP) approach. For this purpose, the cost function aims to penalize any error deviation regarding the inside temperature; which represents the system output; and the control input is penalized as well trying to have the optimal control sequence. Regarding this, the main required key elements to take into consideration for an efficient MPC algorithm design are the model and the optimizer. Figure 5 gives an insight of the proposed regulation and optimization procedure.

- The model is one of the most important components of an MPC algorithm, since it is used to predict the systems behavior when applying a sequence of control commands, in this end, it has to be as specific as possible for MPC aims. It is worth mentioning that for model based predictive control, both the prediction and the control horizons N_p and N_c , that represent respectively the number of predicted future time intervals and the number of control moves for the time interval, are important and have to be

carefully adjusted. Those latests contribute directly in increasing or decreasing both the optimization running and optimization time.

- The optimizer in its part, plays a prominent role in the control approach. Due to Yalmip toolbox used in this framework, the adopted optimizer generates the control activities in the fastest possible way and solves the quadratic programming problem in order to return the optimal solution respecting the constraints on the control notion. In fact, one of the benefits of such a toolbox is that it automatically detects the category of the problem to be solved and optimized in order to select the appropriate solver if available, if it is not the case, the problem is converted to a low level model and then treated and solved.

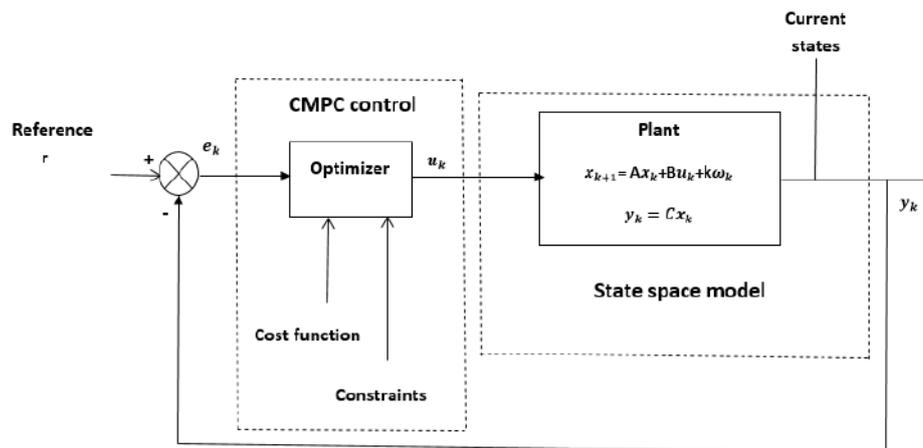


Figure 5. Block diagram of the adopted regulator

In our case of study, single input single output system was taken into account, for this kind of systems, state penalty matrix Q may be chosen regarding the states contribution into the cost function, we are aimed to keep the output at a predetermined level, hence the choice of the state penalization matrix was set to provide a kind of states recalculation into outputs y_k , knowing that $y_k = Cx_k$. For the input penalty R , it is chosen to be small around $R \approx n^{(-2)}$, $n \in N$, and depending on the system input contribution in the cost function, one can fix it to lower or higher values. To recall, the constrained optimization problem used in this framework is based on obtaining the control inputs u_f and u_h , i.e., Fan and heater, where a cost function was selected to be quadratically dependent on the systems error e_k and the control input u_k , under the system dynamics and control constraints. The adopted cost function is presented as follows:

$$\begin{aligned} \underset{u_k}{\text{minimize}} \quad & J = \sum_{k=1}^N e_k' Q e_k + u_k' R u_k \\ \text{subject to} \quad & u_{min} \leq u_k \leq u_{max} \end{aligned} \quad (10)$$

Where $e_k = r - Cx_k$ and r is the reference value. Here, MPC strategy is implemented in a repeated way such that, at each sampling instant k , current states x_k are presents first, then, a sequence of future optimal control predictions is calculated and its first element is extracted and applied back to the plant, hence, for each system model, two MATLAB scripts and a simulation model under Simulink were suggested more specifically:

- Firstly, a MATLAB function file code is created, in which the inputs are defined as: the state and the reference, and a scalar control signal is returned as an output.
- Secondely a Simulink model that includes both the linear state-space model and an the interpreted MATLAB function that holds the MPC controller code is set.
- Thirdly, a setup file regarding the state space model data, is also created.

MATLAB 2018b with Yalmip toolbox of the version '20200116' were used to show the simulation development as presented in section 3. The adopted CDMPC Algorithm using yalmip optimization toolbox for temperature control, can be summarized as follows:

Algorithm 1 CDMPC for Tint control algorithm

Inputs: Current state, current reference

Output: The optimal control inputs u_f or u_h

- 1: Set the systems discrete state space numerical model as in 2.2.1.
- 2: Define and initialize the QP penalty matrices and the MPC prediction horizons for the fan and heater cases
- 3: Identify the reference, states and control as semi definit programming variables
- 4: Initiaize the reference, the objective and constraints
- 5: for $k = 1 : N_f // N_h$
- 6: Solve the optimization problem (10) respecting the constraints along the prediction horizons N_f and N_h
- 7: endfor
- 8: Extract the first element of the optimal control and apply it to the plant.
- 9: end

3. SIMULATION RESULTS AND DISCUSSION

Numerical simulation was carried out in order to evaluate the CDMPC performances. In this regard, MATLAB, Simulink and model predictive control algorithm using YALMIP Toolbox were used in this frame. The optimization problem is solved by above QP algorithm using QUADPROG as a solver. Interpreted Matlab function was used for the controller, and the plant models for simulation purposes under Simulink was engaged as well.

To recall, the objective of the desired control strategy is to maintain the output y_k , i.e., inside temperature T_{int} , as close as possible to the reference value, and try not to exceed posed boundries $15^{\circ}\text{C} \leq T_{int} \leq 25^{\circ}\text{C}$, besides that and for futur real time experiments perspectives, deviding the work in two simulation tasks, i. e., two systems identifications regarding cooling and heating was based essentially on how our system works in real life, i. e., according to the sign of the difference between the setpoint and the measured inner temperature. In order to evaluate the proposed control approach; for both scenarios, i.e., for the fan and heater; the input is constrained to evolve between $0 \leq u_f \leq 4.1$ as voltage applied to the fan and $0 \leq u_h \leq 5$ as voltage applied to the heater. After some trials, the penalty weight factors were chosen scalars as $Q_f = 100$ and $R_f = 0.01$ for the first system and $Q_h = 200$ and $R_h = 0.2$ for the second one, the prediction horizons were set to $N_f = 30$ and $N_h = 40$. For simulation tests, $T_s = 5\text{sec}$ was setted as sample time. Figure 6 describes the evolution of External temperature during 7 minutes, this evolution shows that the external temperature varies between a temperature range $15^{\circ}\text{C} - 17.5^{\circ}\text{C}$.

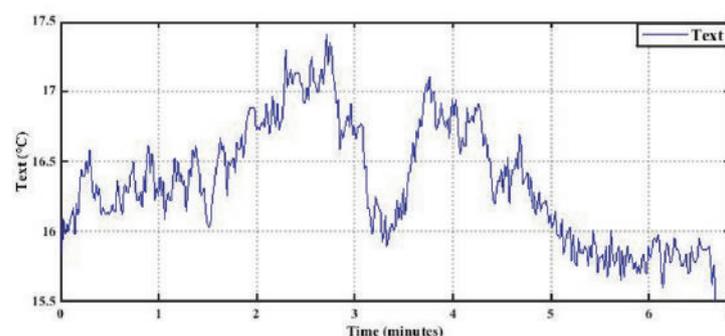


Figure 6. Measured greenhouse external temperature

In one hand, and as presented in Figure 7, it is remarkable that the fans behavior as first actuator, tends to meet the input constraints and more precisely does not exceed 1.5 Volts. Besides, various stopping moments are clearly observed, which contributes to power and energy saving, actuator durability and voltage signal limitation as well. In another hand, Figure 8 shows the the control task performances, which is eventually noticed in the internal temperature setpoint tracking, respecting the desired temperature limits. We can notice that the temperature decreases from 29°C to attend the setpoint variations.

In the same way, Figures 9 and 10 show respectively, the second actuator, i.e., the heater, behavior under constraints and the inside temperature response to the heater input control. As it is visible, the heater

behaves normally respecting the constraints notion and attempts his maximum/minimum voltage power without exceeding the upper and lower bounds constraints limits. In Figure 9 the control mission was obtained, and the temperature evolves and reaches its 22.3°C as first value and then tracks smoothly the setpoint.

It is interesting to note that, the present control strategy regarding the constraints on the control has been evaluated despite some damping comportemnt regarding the setpoint tracking task. In general, one might resume that simulation results using a new optimization toolbox as Yalmip, were succesfully guaranteed. As futur work, various and new are the ideas that has been emerged while working on this article. The first one of them, is the proposed control strategy real time implementation. While the improvement and enhancement of this control method will be taken into account as well. Hoping that these initiatives can lead us to new and interesting results and yields.

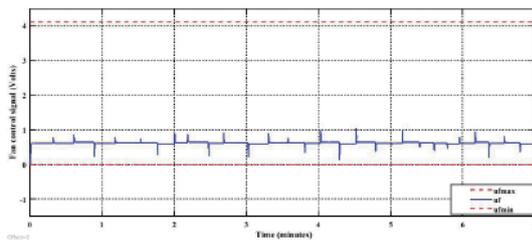


Figure 7. Evolution of the fan control signal under constraints

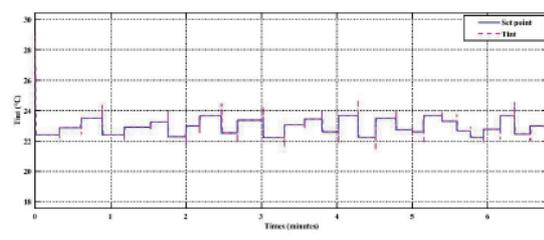


Figure 8. Tint response to the fan as input control "uf"

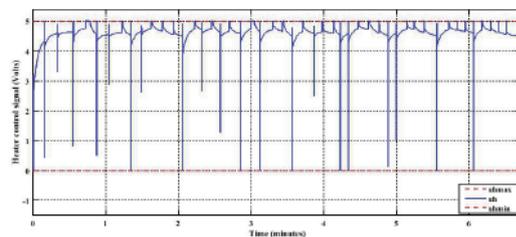


Figure 9. Evolution of the heater control signal under constraints

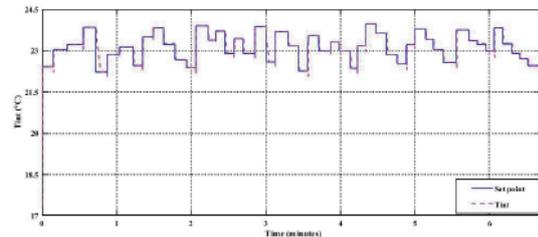


Figure 10. Tint response to the heater input control "uh"

4. CONCLUSION AND FUTURE PERSPECTIVES

In this paper, a constrained discrete model predictive control (CDMPC) for discrete time linear SISO system has been considered. The notion of constraints on the control has been treated as well using quadratic programming (QP) optimization algorithm under a novel toolbox as Yalmip. Necessary and sufficient conditions for the synthesis of the elaborated controller that ensure the desired reference signal tracking and control of inside greenhouse temperature; respecting the constraints of the control inputs condition; have been succesfully accomplished and proved with the above numerical simulations.

We have shown that the control and reference tracking problems are solved for inside temperature of our greenhouse system. The application of these approaches and algorithm can be engaged for other climatic parameter control such as humidity and for multi-input multi-output (MIMO) system as another case of study, in addition to real time implementation, which is one of our perspectives.

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