

Speed profile optimization of an electrified train in cat linh-ha dong metro line based on pontryagin's maximum principle

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ABSTRACT

An urban railway is a complex technical system that consumes large amounts of energy, but this means of transportation still has been obtained more and more popularity in densely populated cities because of its features of high-capacity transportation capability, high speed, security, punctuality, lower emission, reduction of traffic congestion. The improved energy consumption and environment are two of the main objectives for future transportation. Electrified trains can meet these objectives by the recuperation and reuse of regenerative braking energy and by the energy - efficient operation. Two methods are to enhance energy efficiency: one is to improve technology (e.g., using energy storage system, reversible or active substations to recuperate regenerative braking energy, replacing traction electric motors by energy-efficient traction system as permanent magnet electrical motors; train's mass reduction by lightweight material mass...); the other is to improve operational procedures (e.g. energy efficient driving including: eco-driving; speed profile optimization; Driving Advice System (DAS); Automatic Train Operation (ATO); traffic management optimization...). Among a lot of above solutions for saving energy, which one is suitable for current conditions of metro lines in Vietnam. The paper proposes the optimization method based on Pontryagin's Maximum Principle (PMP) to find the optimal speed profile for electrified train of Cat Linh-Ha Dong metro line, Vietnam in an effort to minimize the train operation energy consumption.

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1. INTRODUCTION

Recent years, traffic jam and environmental pollution in metropolitan areas have raised concerns over nations worldwide. Under the circumstances, the urban railway transit seems to be an outstanding solution to reduce the adverse effects of urban mobility because of its large transport capacity, safety, reliability and significantly environmental pollution reduction [1]. In developing countries like Vietnam, dozens of metro lines are going to and getting be built in Hanoi, and Ho Chi Minh cities with a total rout length about 500km. However, metro systems consume huge amounts of energy, proposing saving energy has considerable impacts on the cost reduction for urban railway systems.

There are many ways to reduce the energy consumption in urban railway systems including: recuperating regenerative braking energy through timetable optimization to synchronize braking and accelerating phases of trains [2-11] or using energy storage systems and reversible, active substations to back energy to line utility [12-18]; reducing the losses in power supplies, traction drive system, converters, lines [19-21]; energy-efficient driving by optimizing the speed profile [22-31]. Among these solutions, optimizing the speed profile of each train has been done research extensively [32] because of being suitable for existing metro lines, saving significant energy with relatively low capital investment without improving or building new infrastructure.

All most of metro lines are getting under way in Vietnam not to be equipped regenerative braking energy recuperation devices, and the braking energy will dissipate on braking resistors to cause energy waste. However, using several solutions for saving energy such as: substituting diod recifiers by resersable/active converters in traction substations or installing energy storage devices to recuperate the braking enegy are too expensive and squandered because meterial facilities of the metro lines have just been invested in, so the equipment replacement is not suitable for Metro lines in Viet nam in the comming time. With reasons analysed above, so using the optimal control theory [33] comprising of Pontryagin's Maximum Principle (PMP), Dymamic Programming (DP) [34], Mixed Integer Linear Programming (MILP) [35] finding the optimal speed profile applied to every train is the best solution to minimize the train operation energy consumption without any changes about infrustructure, equipment. The paper proposes one of these methods, namely; using Pontryagin's Maximum Principle for Cat Linh - Ha Dong metro line in Vietnam. Simulation results are presented and showed the effectiveness of optimal control method - PMP in saving energy of train operation up to 10,8%.

2. MODELLING MOTION OF TRAIN

The train is regarded as a particle and kinematic equation can be represented by the following continuous - space model [5]

$$\begin{cases} \frac{dx}{dt} = v \\ mv \frac{dv}{dx} = F_{tr}(v) - F_{br}(v) - W_0(v) - F_{grad}(x) \end{cases} \quad (1)$$

where v, t, x, m represent respectively train speed (m / s), operation time (s), train position (m), full load translating mass of train ($tone$) and $F_{tr}, F_{br}, W_0, F_{grad}$ are traction, electrical braking, resistance, gradient resistance forces applied on the train. These forces are shown in Figure 1.

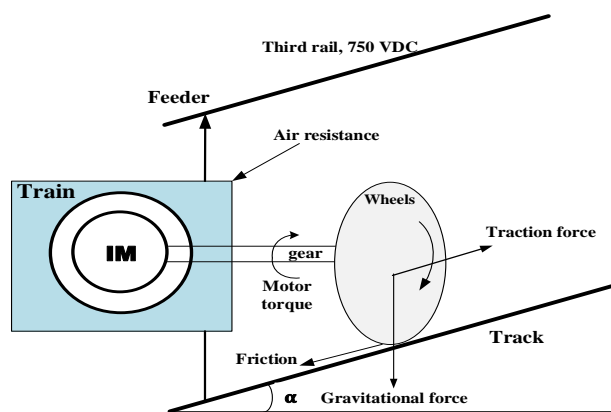


Figure 1. Torques and forces act on the rail wheel

Base on curves of traction force F_{tr} , braking force F_{br} given by manufacturers [36], Using the identification method to find traction, braking characteristic curves in Figure 2, Figure 3, and the Least Square method to find equivalent polynomials.

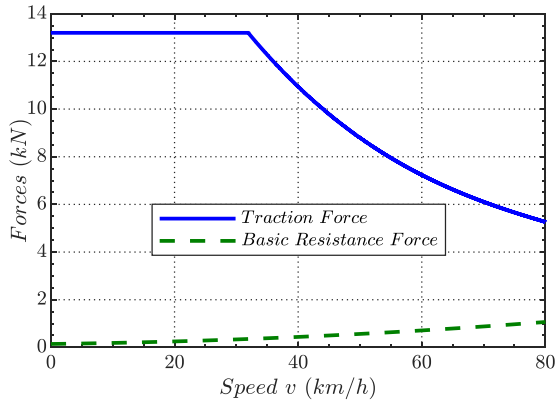


Figure 2. Maximum traction characteristic curve per motor

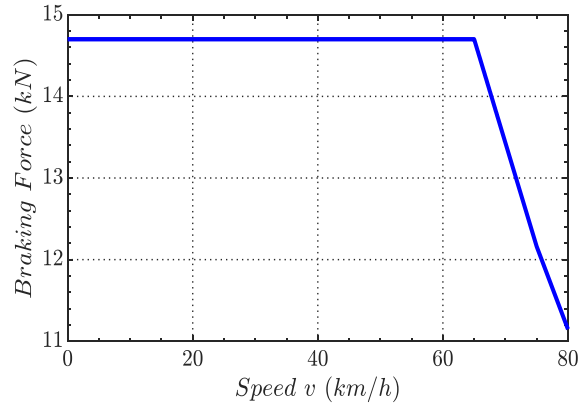


Figure 3. Maximum braking characteristic curve per motor

The maximum traction and maximum braking forces corresponding to the speed v are

$$F_{tr} = \begin{cases} 13.2 & (0 \leq v \leq 32) \\ -2.5 \cdot 10^{-5} v^3 + 0.007 \cdot v^2 - 0.66v + 28.35 & (32 < v \leq 80) \end{cases} \quad (1)$$

$$F_{br} = \begin{cases} 14.7 & (0 \leq v \leq 65) \\ -0.254v + 31.21 & (65 < v \leq 75) \\ -0.2027v + 27.36 & (75 < v \leq 80) \end{cases} \quad (3)$$

Figure 2 shows forces acting on the train in which the resistance force comprises of the air resistance, the friction resistance. The basic resistance w_0 can be calculated by using Davis formula [37]

$$w_0 = \frac{W_0}{m} = a + bv + cv^2 \quad (4)$$

where a, b, c are coefficients of train's resistance.

$$\text{The gradient force } F_{grad} \text{ caused by slope of road: } F_{grad} = mg \sin \alpha \quad (5)$$

where g, α are the gravity acceleration and the rail track slope respectively.

3. SPEED TRAJECTORY OPTIMALITY ANALYSIS BASED ON PMP AND ENERGY ASSUMPTION

Depending on the long or short distance between stations, a train operates in three or four phases. Some studies showed optimal sequence modes of the train to save operation energy; with the short station, the train runs in three phases: accelerating, coasting, braking; with the long station; the train runs in 4 phases: Accelerating, cruising, coasting, braking phase [24], and shown Figure 4, Figure 5. Forces have acted on a train in operation modes are different; accelerating process acted by tractive force, and basic resistance force; cruising process acted by tractive force, and basic resistance force; coasting process has only basic resistance force, braking process with braking force, and basic resistance force.

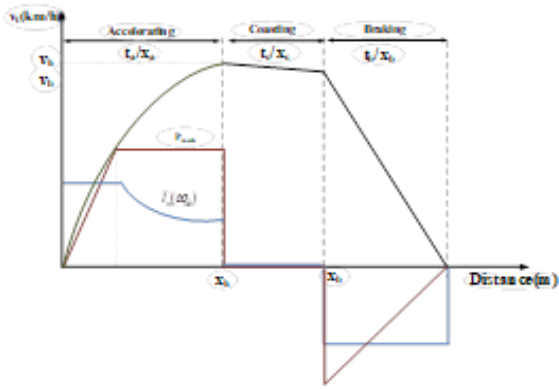


Figure 4. Optimal sequence modes of the train movement with a short station

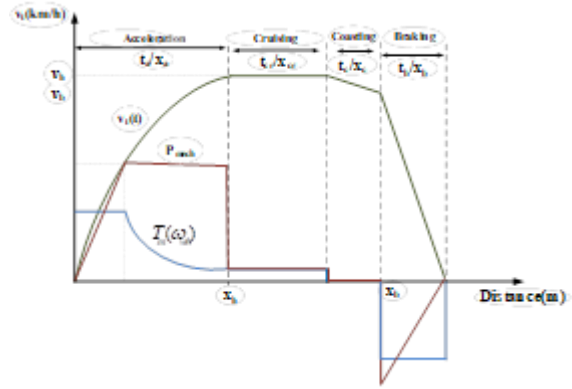


Figure 5. Optimal sequence modes of the train movement with a long station

3.1. Problem formulation

The motion of a train along a track can be described by the state equations [5]

$$\begin{cases} \frac{dt}{dx} = \frac{1}{v} \\ v \frac{dv}{dx} = u_{tr} f_{tr}(v) - u_{br} f_{br}(v) - w_0(v) - f_{grad}(x) \end{cases} \tag{6}$$

where u_{tr}, u_{br} are defined traction and braking control variables of train, both of which are restrained by: $u_{tr} \in [0,1]; u_{br} \in [0,1]; u_{mb} \in [0,1]; f_{tr}, f_{br}, f_{grad}$ are forces per unit mass; traction force applied at the wheels, braking force, mechanical force, gradient force acting on the train.

Therefore, boundary conditions are given by:

$$\begin{cases} v(0) = 0, v(X) = 0, t(0) = 0 \\ 0 \leq v(x) \leq V(x), 0 \leq t(X) \leq T, 0 \leq x \leq X \end{cases} \tag{7}$$

where $V(x)$ is the maximum allowable speed, X is the terminal of the train operation; $v(0), v(X)$ are the speed at the beginning, at the end of the route; T is duration of the trip is also given by the timetable.

The objective is to minimize the train's operation energy consumption as the train runs from location $x = 0$ to location $x = X$ in time T by controlling the traction force, while ignoring electric braking force since regenerative braking energy is not recovered. The objective function is written as:

$$J = \int_0^X u_{tr} f_{tr}(v) dx \rightarrow \min \tag{8}$$

3.2. Solution

By Pontryagin's Maximum Principle finding optimal solutions of an objective function is equivalent to maximizing its Hamiltonian equation. Based on (6), (8), a Hamilton function is formed as:

$$H = -u_{tr} f_{tr}(v) + p_1 \frac{1}{v} + p_2 \left(\frac{u_{tr} f_{tr}(v) - u_{br} f_{br}(v) - w_0(v) - f_{grad}(x)}{v} \right) \tag{9}$$

where p_1, p_2 are adjoint variables.

Adjoint variable differential equations are reformed:

$$\frac{dp_1}{dx} = -\frac{\partial H}{\partial t} = 0 \quad (10)$$

$$\begin{aligned} \frac{dp_2}{dx} = & -\frac{\partial H}{\partial v} = u_{tr} \frac{\partial f_{tr}}{\partial v} + p_1 \frac{1}{v^2} + \frac{p_2}{v^2} [u_{tr} f_{tr}(v) - u_{br} f_{br}(v) - w_0(v) - f_{grad}(x)] \\ & - \frac{p_2}{v} \left[u_{tr} \frac{\partial f_{tr}}{\partial v} - u_{br} \frac{\partial f_{br}}{\partial v} - \frac{\partial w_0}{\partial v} \right] \end{aligned} \quad (11)$$

Define $p = \frac{p_2}{v}$, so $p \cdot v = p_2$. Therefore $\frac{dp_2}{dx} = \frac{d(p \cdot v)}{dx} = p \frac{dv}{dx} + v \frac{dp}{dx}$ (12)

$$\Rightarrow \frac{dp}{dx} = \frac{1}{v} \left(\frac{dp_2}{dx} - p \frac{dv}{dx} \right) \quad (13)$$

Given $\frac{dv}{dx} = \frac{u_{tr} f_{tr}(v) - u_{br} f_{br}(v) - w_0(v) - f_{grad}(x)}{v}$ (14)

Therefore, Hamiltonian function is rewritten

$$H = (p-1)u_{tr}f_{tr} - pu_{br}f_{br} - p(w_0 + f_{grad}) + \frac{p_1}{v} \quad (15)$$

Hamiltonian function is maximized by the following values of u_{tr} and u_{br} :

$$\begin{cases} u_{tr} = 1 & \text{if } p > 1 \\ u_{tr} \in (0,1) & \text{if } p = 1 \\ u_{tr} = 0 & \text{if } p < 1 \end{cases} \quad \text{and} \quad \begin{cases} u_{br} = 0 & \text{if } 0 < p < 1 \\ u_{br} \in (0,1) & \text{if } p = 0 \\ u_{br} = 1 & \text{if } p < 0 \end{cases} \quad (16)$$

From the above analysis, five optimal control laws are designed

- Full power (FP): $u_{tr} = 1, u_{br} = 0$ when $p > 1$
- Partial power (PP): $u_{tr} \in [0, 1], u_{br} = 0$ when $p = 1$
- Coasting (C): $u_{tr} = 0, u_{br} = 0$ when $0 < p < 1$
- Full braking (FB): $u_{tr} = 0, u_{br} = 1$ when $p < 0$
- Partial braking (PB): $u_{tr} = 0, u_{br} \in [0, 1]$ when $p = 0$

Substitute (11), 14 in (13), finding the differential equation for $p(x)$

$$\frac{dp}{dx} = \frac{(1-p)}{v} u_{tr} f'_{tr}(v) + \frac{p}{v} u_{br} f'_{br}(v) + \frac{p}{v} w'_0(v) - \frac{p_1}{v^3} \quad (17)$$

From (10), easily, p_1 is chosen by 0.

Full power mode: $p > 1, u_{br} = 0, u_{tr} = 1$, finding accelerating time t_a , accelerating distance x_a

Using (17).

$$\frac{dp}{dx} = \frac{(1-p)}{v} f'_{tr}(v) + \frac{p}{v} w'_0(v) \quad (18)$$

From (18) finding the differential equation to determine x_a, t_a :

$$\begin{cases} \frac{dx}{dv} = \frac{v}{u_{tr} f_{tr}(v) - w_0(v) - f_{grad}(x)} \\ \frac{dt}{dv} = -\frac{1}{u_{tr} f_{tr}(v) - w_0(v) - f_{grad}(x)} \end{cases} \quad (19)$$

with initial conditions: $x_0 = 0, t_0 = 0$

$$\text{Coasting speed } v_b \text{ is calculated as following [38, 39]: } v_b = \frac{\psi(v_h)}{\varphi'(v_h)} \quad (20)$$

where v_h - hold speed is chosen previously:

$$\varphi(v) = v \cdot w_0(v) = v a + bv + cv^2, \psi(v) = v^2 \cdot w'_0(v) = v^2 b + 2cv \quad (21)$$

From (6) finding the differential equation to determine x_c, t_c :

$$\begin{cases} \frac{dx}{dv} = \frac{v}{-w_0(v) - f_{grad}(x)} \\ \frac{dt}{dv} = -\frac{1}{w_0(v) + f_{grad}(x)} \end{cases} \quad (22)$$

with $t_v = v_h = t_a; x_v = v_h = x_a$

Full braking mode: $u_{tr} = 0, u_{br} = 1, p < 0$, finding braking time t_b , braking distance x_b .

$$\text{Using (17): } \frac{dp}{dx} = \frac{p}{v} f'_{br}(v) + \frac{p}{v} w'_0(v) \quad (23)$$

From (6) finding the differential equation:

$$\begin{cases} \frac{dx}{dv} = \frac{v}{-u_{br} f_{br}(v) - w_0(v) - f_{grad}(x)} \\ \frac{dt}{dv} = \frac{1}{u_{br} f_{br}(v) - w_0(v) - f_{grad}(x)} \end{cases} \quad (24)$$

with $t_v = v_b = t_b, x_v = v_b = x_b$.

In the short journey including three phases: Accelerating → coasting → braking in accordance with control laws: full power – coasting – full braking.

4. SIMULATION RESULTS

The simulation is based on the data of Cat Linh-Ha Dong metro line, Vietnam with simulation parameters of train demonstrated in Table 1, and David's coefficients of train's resistance in Table 2. There are 12 stations, 1 depot, 6 traction substations, and two-side power supply mode. In this paper, simulation results are performed for the first Cat Linh station to the 12th Yen Nghia station with 12.61 km in length [36].

Table 1. Simulation parameters of train

Parameters of Metro Train	Unit	Value
Train gand-up	2M2T	
Full load translating mass	kg	246700
Number of electrical traction unit		08
Max speed	km/h	80
Base speed	km/h	40
Dwell time	s	30
Max acceleration/braking rates	m/s ²	0.94/1

Table 2. David 's coefficients of train's resistance

Parameters	Value
<i>a</i>	$1.19 \cdot 10^{-2}$
<i>b</i>	$2.56 \cdot 10^{-3}$
<i>c</i>	$1.54 \cdot 10^{-4}$

Because the distance among stations in Cat Linh - Ha Dong metro line is short (the shortest station is 902m, the longest one is 1480m), operation modes of electrified train are comprised of accelerating → coasting → braking. Regarding as track conditions, constraints, the speed from a station to another station is different, the slowest speed at 53km/h, the highest speed at 73km/h, but is always smaller than limit speed 80km/h, the optimal trip time is longer 2s indicated in Figure 6 and Figure 7, Table 3. Figure 7 also showed optimal switching points change, so do optimal accelerating, coasting, braking distances significantly. The key result lies in saving energy consumption in optimal speed trajectory up to 10,8% (practical energy consumption is 176,24kWh, while optimal energy consumption attains 157,19kWh).

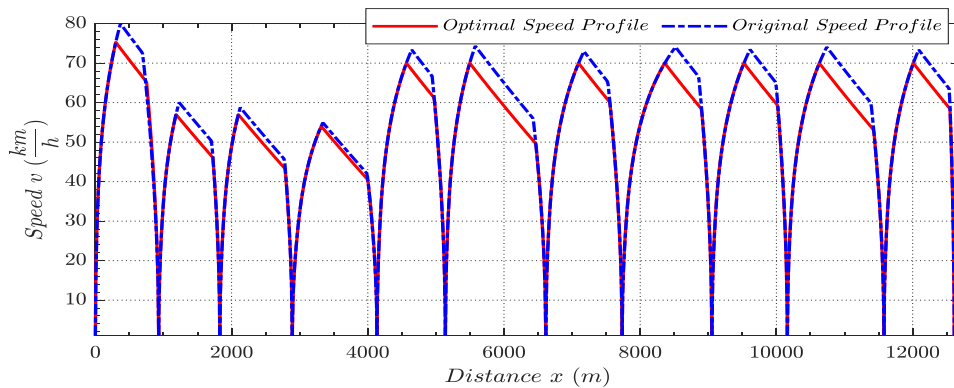


Figure 6. A Comparison of Optimal speed profile and Original speed profile

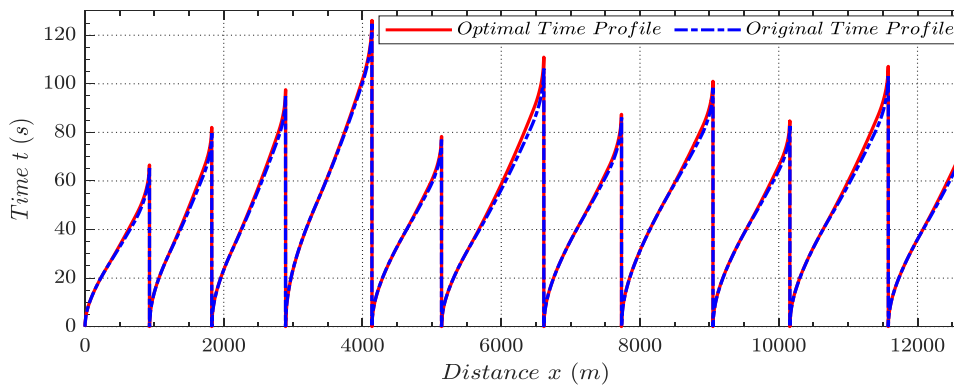


Figure 7. A Comparison of Optimal time profile and Original time profile

Table 3. Results of a comparison of energy consumption with / without energy optimal strategy

Inter-station length	Distance (m)	Practical energy consumption (kWh)	Actual trip time (s)	Optimal energy consumption(kWh)	Optimal trip time (s)
Cat Linh-La Thanh	931	19.5	66	18.59	68
La Thanh-Thai Ha	902	10.94	79	9.7	81
Thai Ha-Lang	1076	10.5	95	9.8	97
Lang-VNU	1248	9.9	124	9.5	126
VNU- Ring Road 3	1010	17.4	77	15.4	78
Ring Road 3-Thanh Xuan	1480	17.4	105	15	107
Thanh Xuan-Ha Dong BS	1121	17.6	86	15.7	87
Ha Dong BS-BV Ha Dong	1324	19.6	98	16.6	100
BV Ha Dong-La Khe	1110	17.8	83	15.7	85
La Khe-Van Khe	1428	18.2	103	15.7	105
Van Khe-Yen Nghia	1032	17.4	72	15.5	74

5. CONCLUSION

After analyzing advantages and disadvantages of solutions for effective energy usage of electrified train operation, the paper focuses on applying Pontryagin's maximum principle to find the optimal speed profile able to saving energy up to 10,8% comparison with the original speed profile. The theoretical approach is verified by simulation results including 12 stations of metro line Cat Linh - Ha Dong, Vietnam with three operation phases: accelerating, coasting, braking. Undoubtedly, using PMP determining the optimal speed profile for metro Cat Linh - Ha Dong is going to set the first step for applying the optimal control theory to other metro lines being construction in Vietnam with target: saving energy.

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