

Direct and indirect vector control of a doubly fed induction generator based in a wind energy conversion system

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ABSTRACT

In the recent years, the development and the exploitation of renewable energy knew a great evolution. Among these energy resources, the wind power represents an important potential for that the wind system has been the subject of several researches. The purpose of this study is to improve the power extracted from wind energy, taking into consideration the variation of wind speed which causes a problem in energy production. For this purpose, we have controlled the powers whether it is active or reactive delivered by the generator. This paper, presents essentially the modeling and control of doubly- fed induction generator (DFIG), which is connected to a variable speed wind turbine. Firstly, the model of the wind power system with the maximum power point tracking (MPPT) strategy is shown. Then, the modeling of doubly- fed induction generator (DFIG) and its power control is presented. Finally, to ensure the attitude of these controls the simulations is presented in the Matlab/Simulink environment.

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1. INTRODUCTION

Following the strong industrialisation, electric energy will always reside an energy that humanity can not do without it. Fossil fuels have long been used in the production of electrical energy, these fossil fuels are causing harmful damage to the environment. [1] To meet the high demand of energy and at the same time keep the environment safe, the majority of countries has opted for the use of renewable energies. These energies are inexhaustible, clean and do not create greenhouse gases unlike fossil fuels. [2][3]

Among the renewable energies, wind energy is experiencing a significant growth and is considered as a mature and economical technology[4]. However, the problem is that this resource is characterized by variable wind speed [5]. For this reason, we have opted for the generator doubly fed induction, as well as other advantages such as; reducing the sizing of the converters, and improving the quality of the energy produced. On the other hand, the control of this machine remains the most important and complex phase.[6][7]

In that way we will start our study by modeling the wind turbine. Then, the MPPT control which ensures an important role to extract the maximum of power. Thereafter, the modeling of the DFIG, and also the power control which is done by the vector control. In terms of this later we have two types: direct field oriented control(DFOC) and indirect oriented field control(IFOC). Finally, the results of the simulations will be presented in the environment Matlab/Simulink in order to conclude the most efficient and robust control also the impact of the MPPT control on the system.

2. MODELLING OF WIND TURBIN

The wind turbine allows the transformation of kinetic energy into mechanical energy and then into electrical energy through a generator. Wind power depends on the surface to be swept (S), wind speed (v) and air density (ρ). Based on the fluid mechanics equations we have the following equation [8][9]:

$$P_v = \frac{\rho \cdot S \cdot V^3}{2} \quad (1)$$

According to Betz's law, a wind turbine can never convert more than 16/27 (or %59) of the kinetic energy of the wind. C_p expresses the aerodynamic efficiency of the wind turbine. It depends on the ratio (λ), and the angle of orientation of the blades (β). The ratio (λ) and C_p are expressed by the following relations [3]:

$$\lambda = \frac{R \cdot \Omega_t}{V} \quad (2)$$

$$C_p(\lambda, \beta) = (0.5 - 0.0167 \cdot (\beta - 2)) \cdot \sin\left(\frac{\pi \cdot (\lambda + 0.1)}{18.5 - 0.3 \cdot (\beta - 2)}\right) - 0.00184 \cdot (\lambda - 3) \cdot (\beta - 2) \quad (3)$$

Where Ω_t is the speed of the turbine, R is the wind turbine radius.

The aerodynamic power, which is converted by a wind turbine depends on the power coefficient C_p , the following equation shows it [2][4]:

$$P_{aer} = C_p(\lambda, \beta) \cdot P_v \quad (4)$$

The following relationship describes the aerodynamic torque

$$T_{aer} = \frac{P_{aer}}{\Omega_t} = C_p(\lambda, \beta) \cdot \frac{\rho \cdot S \cdot V^3}{2 \cdot \Omega_t} \quad (5)$$

In order to adapt the slow speed of the turbine to the speed of the generator, a multiplier is added, this latter is modelled by the following equations [6]:

$$C_g = \frac{C_t}{G} \quad (6)$$

$$\Omega_t = \frac{\Omega_{mec}}{G} \quad (7)$$

Where C_g is the generator torque, Ω_{mec} is the high speed of the generator, G: multiplier gain

From the fundamental equation of the dynamics we can determine the mechanical speed, however the mechanical torque is giving by [5][4]:

$$J \frac{d\Omega_{mec}}{dt} = T_{mec} = T_g - T_{em} - f \cdot \Omega_{mec} \quad (8)$$

Where T_{em} is the electromagnetic torque, T_{mec} is the mechanical torque, f is the viscous friction torque, J is the total inertia.

3. MAXIMUM POWER POINT TRACKING CONTROL

The goal of the MPPT is to optimize the wind energy captured by following the optimal speed. In order to recover as much energy as possible from the wind turbine, we must continuously adapt the mechanical speed of the DFIG to the wind speed. Therefore, it is possible to estimate in real time the value of the wind speed. Then, the electromagnetic torque extracted from the MPPT control is applied to the DFIG to sure that the generator operates at its optimal speed. This diagram as shown in Figure 1 illustrates the wind turbine model with the MPPT control model [3][9]:

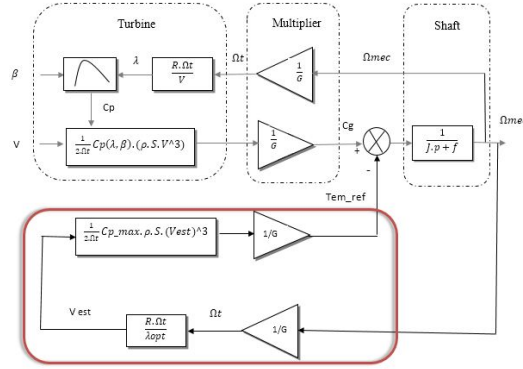


Figure 1. Turbine and MPPT model

The estimated value of the wind speed is given by:

$$V_{est} = \frac{R \cdot \Omega_t}{\lambda_{opt}} \quad (9)$$

The expression of the reference power becomes:

$$P_{aer.ref} = C_{p_{max}}(\lambda, \beta) \cdot \frac{\rho \cdot S \cdot V_{est}^3}{2} \quad (10)$$

The expression of the reference electromagnetic torque becomes:

$$T_{em.ref} = \frac{P_{aer.ref}}{\Omega_t} = \frac{1}{2} \cdot C_{p_{max}}(\lambda, \beta) \cdot \frac{\rho \cdot \Pi \cdot R^5}{\lambda C_{p_{max}^3}} \cdot \Omega_t^2 \quad (11)$$

4. MODELLING OF THE DFIG

The stator of the machine is directly connected to the power grid, but the rotor is connected through the power electronics. The mathematical model of DFIG in the park referential (d-q) is given by the following equations [10][11][12][13]:

V_{sd} , V_{sq} , Φ_{sd} , Φ_{sq} are respectively the equations of the voltages and stator flux in the d-q reference.

$$\begin{aligned} V_{sd} &= R_s \cdot I_{sd} + \frac{d\Phi_{sd}}{dt} - \Phi_{sq} \cdot \omega_s \\ V_{sq} &= R_s \cdot I_{sq} + \frac{d\Phi_{sq}}{dt} + \Phi_{sd} \cdot \omega_s \\ \Phi_{sd} &= L_s \cdot I_{sd} + M \cdot I_{rd} \\ \Phi_{sq} &= L_s \cdot I_{sq} + M \cdot I_{rq} \end{aligned} \quad (12)$$

V_{rd} , V_{rq} , Φ_{rd} , Φ_{rq} are respectively the equations of the voltages and rotor flux in the d-q reference.

$$\begin{aligned} V_{rd} &= R_r \cdot I_{rd} + \frac{d\Phi_{rd}}{dt} - \Phi_{rq} \cdot \omega_r \\ V_{rq} &= R_r \cdot I_{rq} + \frac{d\Phi_{rq}}{dt} + \Phi_{rd} \cdot \omega_r \\ \Phi_{rd} &= L_r \cdot I_{rd} + M \cdot I_{sd} \\ \Phi_{rq} &= L_r \cdot I_{rq} + M \cdot I_{sq} \end{aligned} \quad (13)$$

R_s, R_r : stator and rotor resistances.

L_s, L_r : cyclic stator and rotor Inductances.

M : mutual inductance.

The frequency of the stator voltage is being imposed by the grid, in the opposite the pulsation of the rotor currents is given by:

$$\omega_r = \omega_s - \omega \quad \text{with} \quad \omega = p \cdot \Omega \quad (14)$$

p : Number of pole pairs of the machine.

ω_s, ω_r : Pulse of the stator and rotor electrical quantities respectively .

The Electromagnetic torque is expressed by:

$$T_{em} = p \cdot \frac{M}{L_s} \cdot (\phi_{sq} \cdot I_{rd} - \phi_{sd} \cdot I_{rq}) \quad (15)$$

The Active and reactive stator powers are:

$$\begin{aligned} P_s &= V_{sd} \cdot I_{sd} + V_{sq} \cdot I_{sq} \\ Q_s &= V_{sq} \cdot I_{sd} + V_{sd} \cdot I_{sq} \end{aligned} \quad (16)$$

5. FIELD ORIENTED CONTROL

Vector control is one of the most widely used techniques for controlling electrical machines. It is based on the fact that the machine is similar to a DC machine with separate excitation, this latter ensures a natural decoupling between currents and flux. [14][15]

According to the equation (15) we see clearly the strong coupling between the fluxes and the currents rotoric and statoric which generates a difficulty in the control of the DFigure The principle of vector control is to orient the flux of the machine in one of the two axes d or q. In our case and in order to simplify the control of stator power (active or reactive), we use an orientation on the d axis. [2][12]

However:

$$\Phi_{sd} = \Phi_s \quad \text{and} \quad \Phi_{sq} = 0 \quad (17)$$

The expressions of the electromagnetic torque becomes:

$$T_{em} = -\frac{3}{2} \cdot p \cdot \frac{M}{L_s} \cdot \phi_{sd} \cdot I_{rq} \quad (18)$$

The expressions of the stator voltages becomes:

$$\begin{aligned} V_{sd} &= R_s \cdot I_{sd} + \frac{d\Phi_{sd}}{dt} \\ V_{sq} &= R_s \cdot I_{sq} + \Phi_{sd} \cdot \omega_s \end{aligned} \quad (19)$$

For medium and high power machines, stator resistances are neglected [9], therefore the stator voltage equations become:

$$\begin{aligned} V_{sd} &= \frac{d\Phi_{sd}}{dt} \\ V_{sq} &= \Phi_{sd} \cdot \omega_s \end{aligned} \quad (20)$$

In steady state, it is assumed that the flow is constant, thus:

$$\begin{aligned} V_{sd} &= 0 \\ V_{sq} &= V_s = \Phi_s \cdot \omega_s \end{aligned} \quad (21)$$

$$\begin{aligned} \Phi_{sd} = \Phi_s &= L_s \cdot I_{sd} + M \cdot I_{rd} \\ \Phi_{sq} = 0 &= L_s \cdot I_{sq} + M \cdot I_{rq} \end{aligned} \quad (22)$$

From the equation (22), we deduce the equations linking between stator and rotor currents:

$$\begin{aligned} I_{sd} &= \frac{\Phi_s}{L_s} - \frac{M}{L_s} \cdot I_{rd} \\ I_{sq} &= -\frac{M}{L_s} \cdot I_{rq} \end{aligned} \quad (23)$$

The relations of the powers become :

$$\begin{aligned} P_s &= V_{sq} \cdot I_{sq} \\ Q_s &= V_{sq} \cdot I_{sd} \end{aligned} \quad (24)$$

To express the power relations as a function of the rotor currents, we replace in the previous equation the currents by the equation (23):

$$\begin{aligned} P_s &= -\frac{V_s \cdot M}{L_s} \cdot I_{rq} \\ Q_s &= \frac{V_s^2}{L_s \cdot \omega_s} - \frac{V_s \cdot M}{L_s} \cdot I_{rd} \end{aligned} \quad (25)$$

By replacing flux and stator currents in the equation (13) by the expression (23) we obtain:

$$\begin{aligned} \Phi_{rd} &= (L_r - \frac{M^2}{L_s}).I_{rd} + \frac{V_s.M}{L_s.\omega_s} \\ \Phi_{rq} &= (L_r - \frac{M^2}{L_s}).I_{rq} \end{aligned} \tag{26}$$

In order to control the generator ,these expressions are established showing the relationship between the currents and the rotor voltages that will be applied to it.

$$\begin{aligned} V_{rd} &= R_r.I_{rd} + (L_r - \frac{M^2}{L_s}).\frac{dI_{rd}}{dt} - g.\omega_s.(L_r - \frac{M^2}{L_s}).I_{qr} \\ V_{rq} &= R_r.I_{rq} + (L_r - \frac{M^2}{L_s}).\frac{dI_{rq}}{dt} - g.\omega_s.(L_r - \frac{M^2}{L_s}).I_{dr} + g.\frac{M.V_s}{L_s} \end{aligned} \tag{27}$$

It exists two methods of Field Orientation Control: [16]

5.1. Direct Field Orientation Control (DFOC)

This method consists on regulating the active and reactive stator powers of DFIG independently , by using a PI controller on each axis, while neglecting the coupling terms between the two axes. This method is called direct because the PI controller act directly on the voltages[15][16]; The figure bellow shows the model of direct field orientation control;

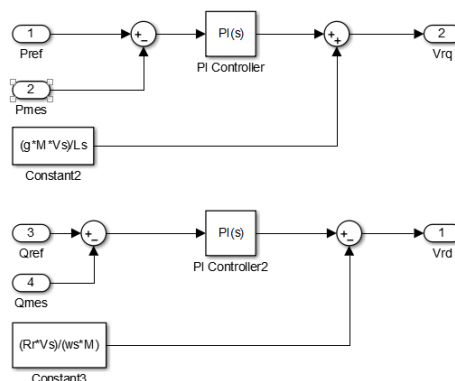


Figure 2. Direct field orientation control

5.2. Indirect Field Orientation Control(IFOCC)

Unlike direct control and in order to regulate the powers as well as the currents rotor. This method takes into consideration the coupling terms and puts two PI controllers on each axis [2].The figure bellow shows the model of indirect field orientation control;

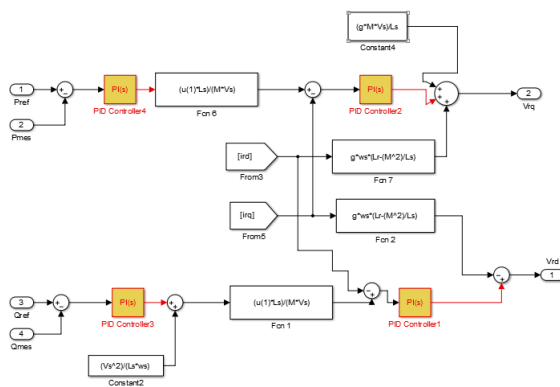


Figure 3. Indirect field orientation control

6. RESULT AND ANALYSIS

The simulation was performed in the Matlab/Simulink environment;

In order to model the wind, we use harmonic sums corresponding to the pulse ω . It is modeled by the following equation:

$$V = V_0 + \sum_{i=1}^n A_i \cdot \sin(\omega_i t + \Phi_i) \quad (28)$$

After applying a random wind profile as shown in 4, from the as shown in 5 and as shown in 6, it is clear that the system with MPPT control has the coefficient of power C_p maintained at its maximum value $C_p=0.5$ and the Paer correctly follows the wind speed, unlike the system without MPPT control. As well as as shown in 7 illustrates the ratio λ which is equal to its optimal value.

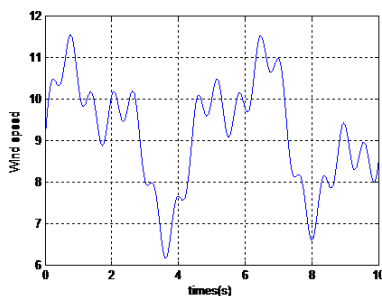


Figure 4. Wind speed

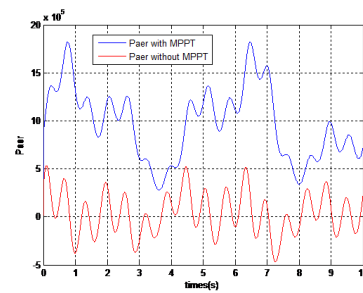


Figure 5. Aerodynamic power

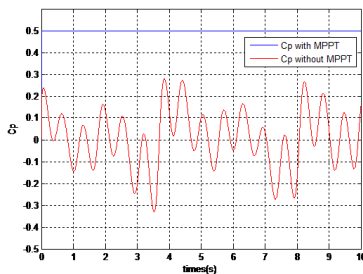


Figure 6. Cp coefficient

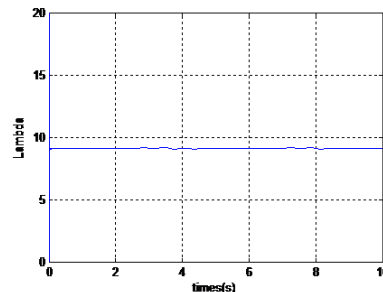


Figure 7. The ratio λ

To visualize the behavior of the system controls and to be able to compare between the two commads we applied an active and reactive power steps. The active and reactive power steps, which are applied to each type of control, are shown in Table 1.

Table 1. Active and Reactive Power Steps

Times(s)	Ps(MW)	times(s)	Qs(MVar)
0 to 0,4	-0.6	0 to 0,2	-0.6
0,4 to 1,5	-1	0,2 to 1,5	-1
1,5 to 2,5	-1.2	1,5 to 10	-1.2
2,5 to 10	-4		

The Figure8 and Figure9 show the active and reactive power with direct control, then Figure10 and Figure11 show rotoric current I_{rd} ant I_{rq} .

The Figure12 and Figure13 show the active and reactive power with indirect control, and then Figure14 and Figure15 show the rotor current I_{rd} and I_{rq} .

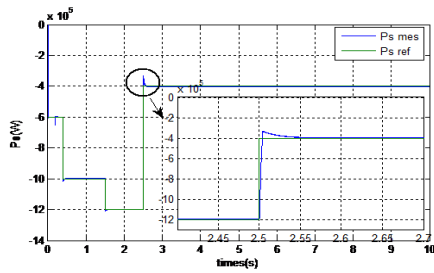


Figure 8. Ps of DFOC

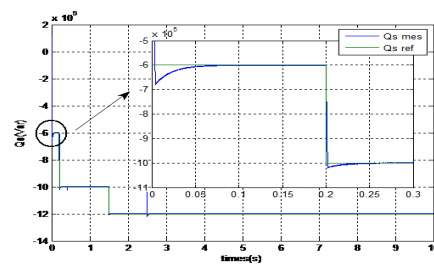


Figure 9. Qs of DFOC

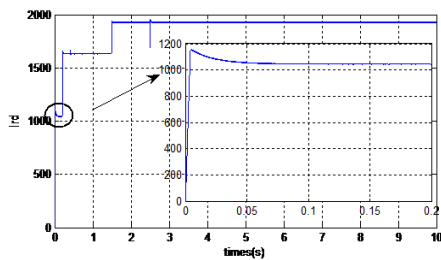


Figure 10. Ird of DFOC

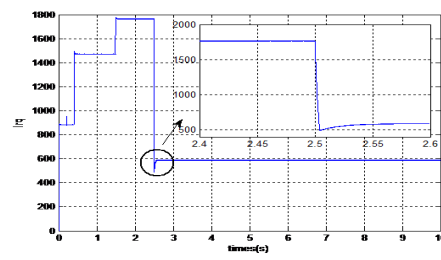


Figure 11. Irq of DFOC

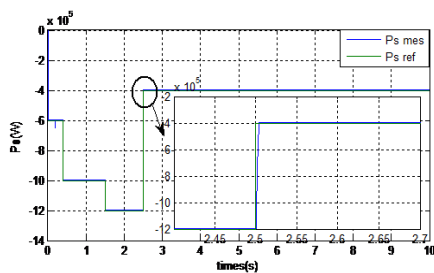


Figure 12. Ps of IFOC

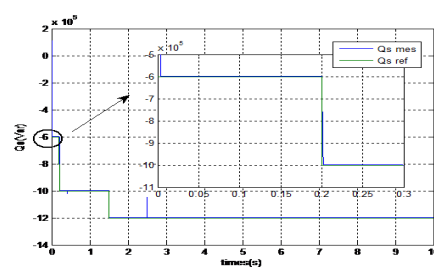


Figure 13. Qs of IFOC

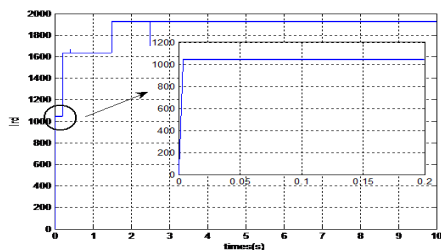


Figure 14. Ird of IFOC

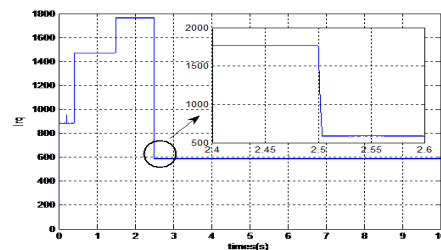


Figure 15. Irq of IFOC

From the previous figures we can see that, active stator power (P_s) depend on the quadrature rotor current (I_{rq}), and also reactive stator power (Q_s) depend on the direct rotor current (I_{rd}). So in both cases (DFOC, IFOC) the decoupling is perfectly ensured.

In the same figures; the system follows the applied instructions except that at the level of the indirect field oriented control we can see very well that, it follows the instruction better than the direct control either for the powers or the currents.

The following table summarizes the comparison of the two types of control in terms of response time (T_r) and Overtaking (O). It is seen that the IFOC control lead to good tracking performance.

Table 2. Difference between DFOC/IFOC

	Direct		Indirect	
	Rt(ms)	O%	Rt(ms)	O%
Ps	50	17,5	3	0
Qs	60	13,3	5	0
Ird	50	9,52	4	0
Irq	60	16,66	4	0

7. CONCLUSION

this article deals with the improvement of the power generated from a wind power system. After modeling the whole system (wind turbine and DFIG generator) ,firts of all , we started with MPPT control to ensure maximum power extraction by fixing C_p at its maximum value . After that, we are interested in vector control which consists in making the machine similar to a DC machine. Finally, we have have compared the two types of control DFOC and IFOC . In order to validate our study, we have carried out the simulation in the Matlab/Simulink environment .

Based on the simulation results, the MPPT control allows us to exploit the maximum of wind energy to produce the maximum of electrical energy. Also, the vector control is applied carefully . Moreover, we constated that, direct control which is based only on power regulation, is the easiest to implement but not the most efficient. On the other hand, the indirect control where the currents are also controlled is a little complex to implement, but, it ensures a good tracking of the instruction and allows us to have an optimal performance of the system.

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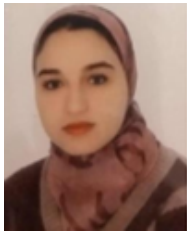
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