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Performance Evaluation of two Port and four Port Measurement for Twisted Pair Cable

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ABSTRACT

A balance-unbalance (balun) transformer is commonly used to connect the balance 100 Ohm twisted pair cable to the unbalance 50 Ohm network analyzer ports, but due to the limitations of the core (i.e. ferrite) inside the balun, the balun can only effectively operates at a certain band of frequencies. This limitation can be eliminated by using a 4-port vector network analyzer (VNA) which is done by connecting the VNA's ports to each conductor end. The extracted S-parameters will then be transformed to a 2-port S-parameters in differential mode at both ports. To validate the measurement technique, S-parameter measurement by using the 4-Port Network Analyzer without any balun will be compared to the measurement which used the 2-Port Network Analyzer with the balun transformers. Two twisted pair cable distances are selected as reference which are 500, and 1000 meters with nominal copper diameter of 0.5mm. Based on the measurement results, the 4-ports measurement shows good correlation with the 2-ports measurement especially at 500m distance. This shows that the 4-ports measurement setup is suitable to be used to measure twisted pair copper cable and possible to measure at a higher frequency band such as up to 500 MHz but at a shorter twisted pair cable distance.

2624

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1. INTRODUCTION

Twisted pair cable was invented and patented by Alexander Graham Bell in the 1880s [1] to transmit voice over the wire. Since then, the function of twisted pair copper has changed from voice to facsimile and in the last decade the twisted pair is widely used to transmit digital data alongside with fibre cable. Eventhough a study by [2] stated that twisted pair may have less effect on reducing external noise, the claim can only be true for short distances only, but for long distances, the effect of reducing external noise is greatly noticeable. Twisted pair cable was thought going to end with the ISDN technology which can only carry data rate speed below 1 Mbps, but then Asymetric Digital Subscriber Line, ADSL was introduced in the early 1990s and was then standardize in 1999 in ITU-T [3]. Later, the DSL family expanded with High-Speed Digital Subscriber Line, HDSL, Symetrical High-Speed Digital Subscriber Line, SHDSL, Very High-Speed Digital Subscriber Line, VDSL, VDSL2 [4] and the latest addition, Gigabit Fast Access to Service Terminals, G.fast [5] which after several trials have shown potential of delivering aggregated data rate up to 1Gbps [6]. As stated by [7], with current advancement of copper technology, it is difficult to phase out copper entirely from the service provider network. The capability of high data rate being offered by the mentioned xDSL technologies is only limited to the length of the twisted pair cable, such as ADSL2+ can

offer up to 20Mbps with coverage distance of 5km, VDSL2 can offer up to 50Mbps with coverage distance of 2kmand G.fast can offer up to 1Gbps aggregated data rate with coverage distance of 250m [8]. The trade-off between data rate and coverage distance is an unavoidable limitation which commonly faced in wireless technology environment.

One way to estimate the capacity of any transmission medium is by measuring the scattering parameters (S-parameters) of the medium, take twisted pair cable for example. The S-parameter is able to describe the electrical properties of a device with any number of ports opening by observing the power coming in and out from the ports available in the device [9]. The S-parameter can be used to extract the primary parameters of the device such as twisted pair cable to observe the RLGC values of the cable [10]. An example of how the S-parameters is achieved in a two-port device is as shown in Figure 1 where S11 is obtained by observing the ratio of power coming out to port A to the power coming in from port A. While S21 is achieved by observing the ratio of power coming out to port B to the power coming in from port A. S21 is closely related to the channel capacity of the medium and the S-parameter is usually defined in decibel, dB unit. Equation (1) summarizes the S-parameter equation in relation to the power in and out of the ports. For a four-port device as shown in Figure 2, the S-parameter will be more complex as it will generate a four-by-four matrix as shown in Equation (2).



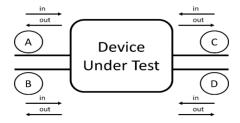


Figure 1. S-parameter for two ports

Figure 2. S-parameter for four ports

$$S_{11} = \frac{A_{out}}{A_{in}} \quad S_{12} = \frac{A_{out}}{B_{in}}$$

$$S_{21} = \frac{B_{out}}{A_{in}} \quad S_{22} = \frac{B_{out}}{B_{in}}$$

$$S_{11} = \frac{A_{out}}{A_{in}} \quad S_{12} = \frac{A_{out}}{B_{in}} \quad S_{13} = \frac{A_{out}}{C_{in}} \quad S_{14} = \frac{A_{out}}{D_{in}}$$

$$S_{21} = \frac{B_{out}}{A_{in}} \quad S_{22} = \frac{B_{out}}{B_{in}} \quad S_{23} = \frac{B_{out}}{C_{in}} \quad S_{24} = \frac{B_{out}}{D_{in}}$$

$$S_{31} = \frac{C_{out}}{A_{in}} \quad S_{32} = \frac{C_{out}}{B_{in}} \quad S_{33} = \frac{C_{out}}{C_{in}} \quad S_{34} = \frac{C_{out}}{D_{in}}$$

$$S_{41} = \frac{D_{out}}{A_{in}} \quad S_{42} = \frac{D_{out}}{B_{in}} \quad S_{43} = \frac{D_{out}}{C_{in}} \quad S_{44} = \frac{D_{out}}{D_{in}}$$

$$(2)$$

This paper aims to validate the use of coaxial-to-DE9 (D-subminiature electrical connector for 9-pin) adaptor locally made in-house during the S-parameter measurement by comparing S21 results of the coaxial-to-DE9 adaptor versus on the shelf balun transformer. The comparison was made by using root mean square error, RMSE method to quantify the deviation between both setup of measurement as being used in [11].

2. RESEARCH METHOD

In this section, the process of calibration and measuring the S-parameters by using the two-port Network Analyzer and four-port Network Analyzer is explained. The measurement involved three stages as shown in Figure 3, which are the setup of cable and equipment, measurement execution and the post-processing of the S-parameter results and the correlation study.

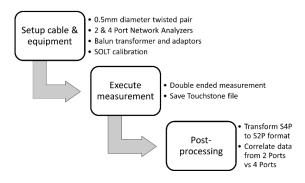


Figure 3. Overall flow of the measurement

2.1. Cable under test

Telekom Malaysia twisted pair cable will be used for the test with cable distance of 500m and 1000m. The type of twisted pair cable used in the test is the overhead type with integral bearer with conductor diameter of 0.5m. Five different cable conditions was set to emulate the conditions which is possible to happen in the TM cable network as shown in Table 1.

Cable Condition	Cable setup	Diagram
Ideal	Normal cable condition	XXXXXX
Bridge Tap	Parallel wiring, T- junction setup usually occurred at the customer's premise	××××××××××××××××××××××××××××××××××××××
Open	One of the conductor of the twisted pair is cut open at any part of the cable	Open
Short	The two conductor is shorted at any part of the cable	Short
Uneven Length	One of the conductor of the twisted pair has additional cable length at any part of the cable	Additional length

Table 1. Cable Conditions Emulated for the S-Parameter Test

Each of the cable's end was soldered to DE9 male connector as shown in Figure 4. Each end of the twisted pair conductor was soldered to pin number 5 and 9 only. Once soldered, the connectivity of each conductor was tested with digital multi-meter.

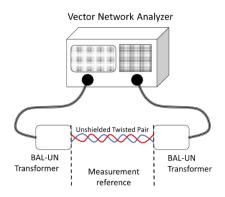


Figure 4. DE9 male connector

2.2. Measurement setup

The two-port measurement as shown in Figure 5 includes two balun transformers made by North Hills, model NH14211 with operating frequency from 100 kHz to 350 MHz. The four-port measurement as

shown in Figure 6 uses a custom made coaxial-to-DE9 adaptor which links the four coaxial cables to each of the twisted pair cable's end. The two and four port measurement was done by using Keysight (formerly known as Agilent) E5071C Network Analyzer. The measurement setting on the network analyser is as follows: start frequency at 9 kHz; stop frequency: 500 MHz and sampling number: 10000 points.



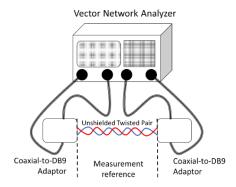
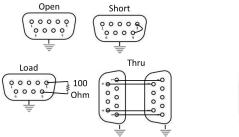


Figure 5. Two-port measurement setup

Figure 6. Four-port measurement setup

2.3. Calibration process

Both two-port or four-port measurement used the Short-Open-Load-Thru (SOLT) calibration method. The calibration kit was customised for DE9 connector. As shown in Figure 7, the two-port measurement, there are four calibration kit, which are the Short, Open, Load and Thru, while for the four-port measurement, the only difference from the two-port is the Thru kit will have 5 configurations as shown in Figure 8.



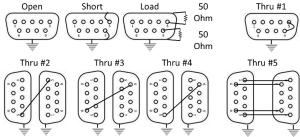


Figure 7. Calibration kit for two-port measurement

Figure 8. Calibration kit for four-port measurement

2.4. Conversion from S4P file to S2P file

The result that will be compared between the two-port and the four-port is the S21 parameter in dB unit. But before the comparison can be made, the S4P file need to be converted to S2P file. This can be done easily if the built-in function in Matlab software, S2SDD is used, which is available in the RF Toolbox. Without the use of the Matlab built-in function, the data can also be converted by following Equation (3) as mentioned in [12]. Once the S4P have been converted, the result of the S21will be compared by using root mean square method which can be calculated by using Equation (4), where A is the value of the S21.

$$S_{dd11} = \frac{S_{11} - S_{12} - S_{21} + S_{22}}{2}$$

$$S_{dd12} = \frac{S_{13} - S_{14} - S_{23} + S_{24}}{2}$$

$$S_{dd21} = \frac{S_{31} - S_{32} - S_{41} + S_{42}}{2}$$

$$S_{dd22} = \frac{S_{33} - S_{34} - S_{43} + S_{44}}{2}$$
(3)

$$RMSE = \sqrt{\frac{\sum_{f_1 - f_N} [A_{S4P} - A_{S2P}]^2}{N}}$$
 (4)

3. RESULTS AND ANALYSIS

After the measurement for both two-port and four-port were completed, the four-port measurement will need to be converted to S2P format first. The conversion process will follow Equation (3) rule as mentioned in the previous chapter. The results and discussion chapter is presented in four parts. The first and second part is the 500m and 1000m S21 comparison between the two-port and four-port measurement. The third part is the root mean square error calculation tabulation between every cable conditions. Lastly, the results comparison will be discussed and the hypothesis drafted in introduction will be concluded.

3.1. 500m result comparison

Figure 9 to Figure 13 shows the results for the five different cable conditions. For 500m, it is observed that most of the cable condition gives workable operating frequency (value S21 higher than -60dB) up until 30 MHz. It is also spotted that the measurement will began to deviate more after 45 MHz where the S2P measurement notch up a bit than the S4P measurement.

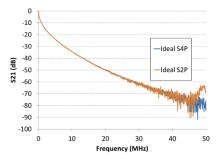


Figure 9. Result comparison for 500m ideal cable condition

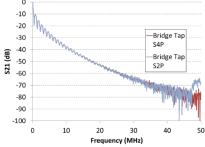


Figure 10. Result comparison for 500m Bridge Tap cable condition

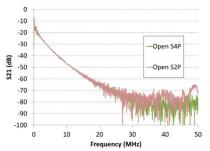


Figure 11. Result comparison for 500m Open cable condition

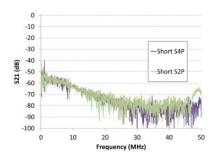


Figure 12. Result comparison for 500m Short cable condition

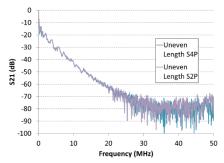
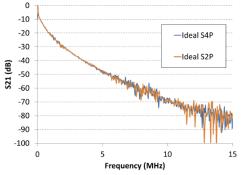


Figure 13. Result comparison for 500m Uneven Length cable condition

3.2. 1000m result comparison

Figure 14 to Figure 18 shows the results for 500m distance, which is observed that most of the cable condition gives workable operating frequency (value S21 higher than -60dB) up until 7 MHz. The S21 values for 1000m are as expectedly much lower than the 500m S21 value. The ripple effect on the bridge tap condition can still be observed at 1000m.



-80 -90 -100 0

(dB)

-60 -60

0

-10

-20

-30

-40

-50

-70

Figure 14. Result comparison for 1000m ideal cable condition

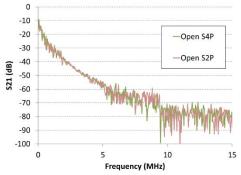
Figure 15. Result comparison for 1000m bridge tap cable condition

Bridge Tap S4I

Bridge Tap S2I

15

10



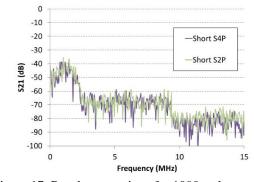


Figure 16. Result comparison for 1000m open cable condition

Figure 17. Result comparison for 1000m short cable condition

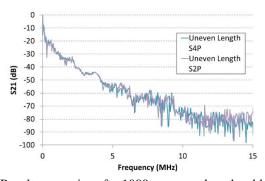


Figure 18. Result comparison for 1000m uneven length cable condition

3.3. Root mean square error calculation and comparison

By using Equation (4), the RMSE for each cable condition was calculated, tabulated and shown in Figure 19 and Figure 20 for distance of 500m and 1000m respectively. It is observed that the RMSE value are consistently high if the RMSE calculation was made by considering the whole frequency band (up to 500 MHz). The RMSE value also decreases along with reduction of maximum operating frequency from 500 MHz to 50 MHz (for 500m distance) or 15 MHz (for 1000m distance) and lastly to 5 MHz. The RMSE value for Short condition is consistently high at both distance as the overall value of S21 deteriorate much faster than other cable condition even at maximum operating frequency of 5 MHz.

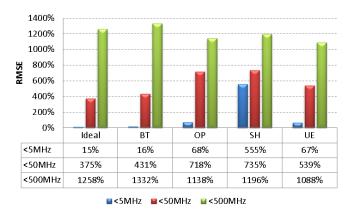


Figure 7. Root mean square error result comparison for 500m against the cable conditions

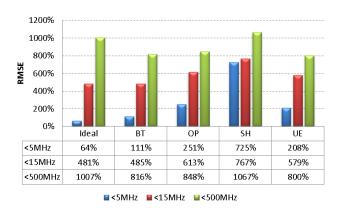


Figure 8. Root mean square error result comparison for 1000m against the cable conditions

3.4. Discussion

The frequency selection of 50 MHz for 500m and 15 MHz for 1000m was based on the workable frequency observed earlier in Figure 9 to Figure 18. The frequency 5 MHz was selected to have the same reference frequency for both distance of 500m and 1000mso that apart from having different distance, any other variables are set to be the same.

At operating frequency below 5 MHz, Ideal condition gives the best RMSE value of 15% for 500m and 64% for 1000m while Short condition gives the worst RMSE value of 555% for 500m and 725% for 1000m. All S21 values for conditions other than Ideal are much lower than Ideal condition due to the impairment emulated to the twisted pair cable. Significant ripples are detected for Bridge Tap condition which is caused by the stub introduced in the somewhere in the middle of the cable.

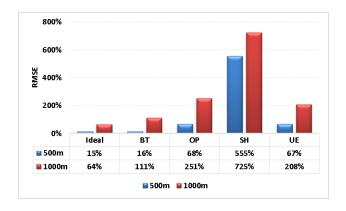


Figure 9. RMSE result comparing S_{21} value against the cable conditions below 5 MHz

It is observed that as the cable distance increase, the RMSE value will increase due to the increase of attenuation level across the frequency and thus reducing the workable operating frequency. As shown in Figure 21, even when comparing the RMSE for operating frequency below 5 MHz, the deviation at 1000m distance is consistently higher than the measured 500m distance. The RMSE value below than 30% is considered good as referred to the RMSE threshold set in [13].

4. CONCLUSION

Based on the measurement results, the 4-ports measurement shows good correlation with the 2-ports measurement especially at 500m distance. This shows that the 4-ports measurement setup is suitable to be used to measure twisted pair copper cable and possible to measure at a higher frequency band such as up to 500 MHz but at a shorter twisted pair cable distance. This will enable the possibilities to study the potential of copper cable for higher transmission rate up to 1 Gbps data rate speed by knowing its primary and secondary property's behaviour at higher frequency bands.

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Mohamad Kamal A Rahim received the B Eng. degree in Electrical and Electronic Engineering from University of Strathclyde, UK, in 1987. In 1989, he joined the Department of Communication Engineering, Faculty of Electrical Engineering Universiti Teknologi Malaysia Kuala Lumpur as an Assistant Lecturer A. He obtained his M.Eng Science from University of New South Wales Australia in 1992 and PhD degrees in Electrical Engineering from University of Birmingham UK in 2003. After he received his Master he was appointed as a Lecturer at Faculty of Electrical Engineering. Now he is the Professor in RF and Antenna at Faculty of Electrical Engineering Universiti Teknologi Malaysia. Some of his research interest includes the areas of design of dielectric resonator antennas, microstrip antennas, RFID antennas for readers and tags, microwave circuits, EBG, artificial magnetic conductors, metamaterials, phased array antennas, computer aided design for antennas, and design of millimeter wave antennas. He has published over 300 articles in journals and conference papers.