

Design of an Interdigital Structure Planar Bandpass Filter for UWB Frequency

S. M. A. Motakabber, M. N. Haidari

Departement of Electrical and Computer Engineering, International Islamic University Malaysia, Malaysia

Article Info

Article history:

Received Jan 2, 2018

Revised Mar 19, 2018

Accepted Mar 28, 2018

Keyword:

Microstrip filter

Microwave substrate

Planar filter

Rreturnloss

Ultra-wideband technology

ABSTRACT

A new topology of miniaturized interdigital structure microstrip planar bandpass filter for Ultra-Wideband (UWB) frequency has been discussed in this paper. The proposed design and its simulation have been carried out by using an electromagnetic simulation software named CST microwave studio. The Taconic TLX-8 microwave substrate has been used in this research. The experimental result and analysis have been performed by using the microwave vector network analyzer. The experimental result showed that the -10dB bandwidth of the filter is 7.5GHz. The lower and upper corner frequencies of the filter have been achieved at 3.1GHz and 10.6GHz respectively. At the center frequency of 6.85GHz, the -1dB insertion loss and the -7dB return loss have been observed. The simulated and experimental results are well agreed with a compact size filter of $19 \times 21 \times 0.5 \text{mm}^3$.

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Corresponding Author:

S. M. A. Motakabber,
Departement of Electrical and Computer Engineering,
International Islamic University Malaysia,
53100 Kuala Lumpur, Malaysia.
Email: amotakabber@iium.edu.my

1. INTRODUCTION

Potential applications of the UWB technology are, position measurement, short-range high-speed wireless communication, rescue radar systems, medical applications and so on [1]. Since 2002, the UWB technology has been regulated by the Federal Communications Commission (FCC) rules; hence any kind of design in this band must follow the FCC guidelines. Microstrip planar bandpass filter is an important component of the UWB system, which can be easily made under FCC regulations. A microstrip bandpass filter can offer extensive performance in the UWB communication. It is capable to select the required band and separating the different frequency ranges as the requirements. A microstrip line is a simple type of the transmission line which can be easily fabricated, miniaturized and connected with the microwave components [2].

In recent times, UWB bandpass filter is widely used in high-speed wireless data communication system because of its excellence [3]. In order to have a compact, cost-effective and easy integration with other microwave components the microstrip waveguide is one of the better options for designing a bandpass filter. Due to the huge potential, in recent times, many academic, research institutions and industries have focused on UWB technology. Various types of UWB microstrip filters are designed and developed. A bandpass filter with dual notched behaviour is reported in [4], a novel UWB bandpass filter is designed in [5], UWB filter with DGS is developed in [6], the U-shaped slot coupling structure is designed in [7] and UWB bandpass filter with CPW structure is developed in [8].

Though these filters have flat passband, low insertion loss and compact in size, however, most of these cover beyond the UWB frequency range. Consequently, they make interference with the licensed

frequencies [6]-[9]. Hence still, efforts have been going on to design the filters with the capability of covering the entire UWB frequency range.

This article proposes a new structure of interdigital finger type microstrip bandpass filter that will cover the full range of UWB frequency only and do not interfere with any other band of frequency and devices. In addition, this compact planar structure bandpass filter provides a low insertion and return loss characteristics which are suitable for UWB application.

2. FILTER DESIGN METHOD

The interdigital coupled line resonator with shunt stubs and square pads are used in the proposed Ultra-wideband bandpass filter. The interdigital resonators are used due to their high coupling degree [4]. The lengths of resonators according to Equation (3) are quarter wavelength ($\lambda/4$) at center frequency of 6.85GHz. However, their lengths are varied to obtain the optimum result. The shunt stubs and square pads provide good lower passband. Varying the size of the two pads will vary the lower passband of the frequency response.

In order to design the bandpass filter a number of mathematical equations are used to calculate the filter parameters, the general formulas [8] are as follows.

Considering $W/h \leq 1$ (width to substrate ratio) and the substrate dielectric constant ϵ_r , the effective dielectric constant can be calculated by using the following formula.

$$\epsilon_{re} = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \left\{ \left(1 + 12 \frac{h}{W} \right)^{-0.5} + 0.04 \left(1 - \frac{W}{h} \right)^2 \right\} \quad (1)$$

The characteristic impedance also can be calculated using the following equation.

$$Z_0 = \frac{\eta}{2\pi\sqrt{\epsilon_{re}}} \ln \left(\frac{8h}{W} + 0.25 \frac{W}{h} \right) \quad (2)$$

Where, the free space wave impedance is $\eta = 120\pi$ Ohms.

The effective dielectric constant is then used to calculate the lengths L (mm) of the resonators of the filter by using the Equation (3).

$$L = \frac{300}{4 \times f \sqrt{\epsilon_{re}}} \quad (3)$$

Where, f is the center frequency of GHz.

However, in order to get the optimum response, the lengths of the resonators should be slightly varied.

The coupling coefficient $M_{i,i+1}$ can be calculated by using Equation (4).

$$M_{i,i+1} = \frac{FBW}{\sqrt{g_i g_{i+1}}} \quad (4)$$

Where, the values of g_i can be found in [8] and FBW is the fractional bandwidth that can be calculated using Equation (5).

$$FBW = \frac{f_U - f_L}{f_c} \quad (5)$$

The Taconic TLX-8 substrate has been used in this filter design which relative permittivity and thickness are 2.55 and 0.5mm respectively. The total size of the bandpass filter is $19 \times 21 \times 0.5 \text{mm}^3$. The transmission line length L_1 and width W_1 are 4.75mm and 1.34mm, respectively, which gives 50Ohm characteristic impedance. The L_2 is 8mm which is almost quarter wavelength based on Equation (3) and its width is, $W_2 = 0.28\text{mm}$; the length of L is 8.25mm and its width is W_2 . The spacing between the fingers is $S = 0.25\text{mm}$; spacing between the fingers is very significant because the coupling between the resonators highly depends on the spacing; although due to the limitations of fabrication machine used to fabricate the filter; to make very small spacing is difficult. The length of the shunt stubs L_3 is 7mm and its width W_3 is 0.25mm; as well as the size of square pads is $4.7 \times 4.7 \text{mm}^2$. The shunt stubs and squared pads together act as an inductor and capacitor effect [3] respectively as a result, it helps to select a desired lower cutoff frequency easily. The ground plane and the microstrip lines of the filter are a copper plate and their thickness is 0.05mm. Figure 1 shows the schematic design of the filter.

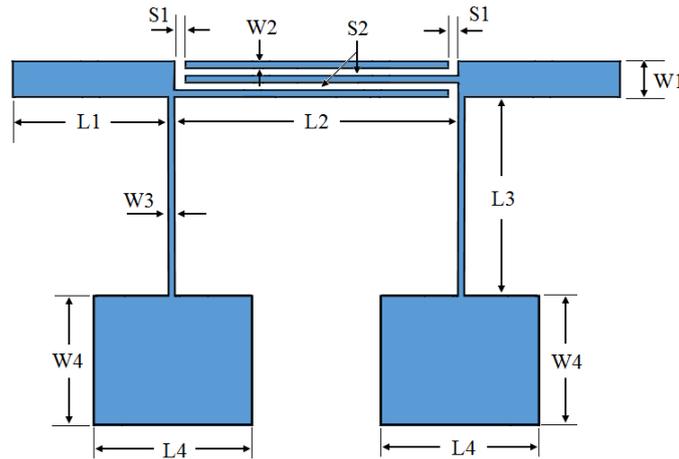


Figure 1. Layout of the UWB bandpass filter

The dimensions of the filter parameters are summarized in Table 1.

Table 1. Dimension of the Filter Parameters

Filter parameter	Value (mm)	Filter parameter	Value (mm)
L_1	4.75	W_1	1.34
L_2	8.25	W_2	0.28
L_3	7	W_3	0.25
L_4	4.7	W_4	4.7
S_1	0.25	S_2	0.25

3. RESULTS AND ANALYSIS

This section illustrates the simulation result of the bandpass filter. The Ultra-wideband microstrip bandpass filter is designed and simulated with CST Microwave Studio; Figure 2 shows the simulation result of the insertion loss S_{21} and return loss S_{11} of the filter respectively.

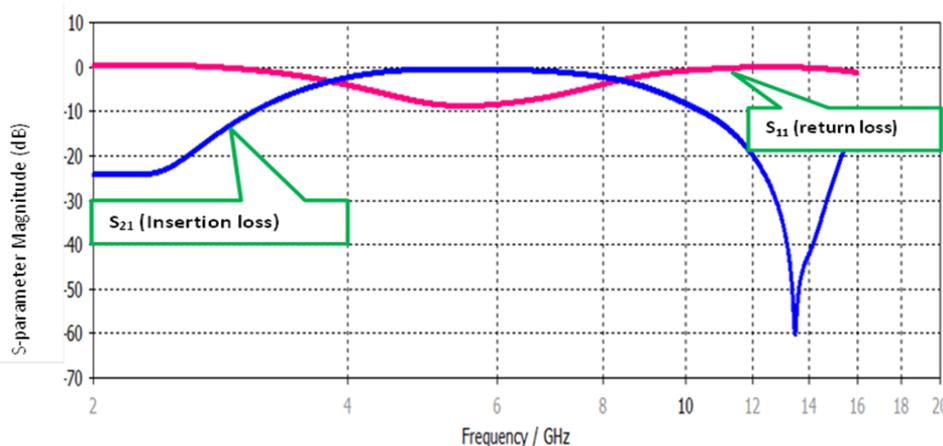


Figure 2. Simulation result of the insertion and return losses of the filter

The 10dB bandwidth of the simulation result is 7.5GHz, which covers the frequency ranges from 3.1GHz to 10.6GHz. As the result, the proposed design does not interfere with any other devices. The center frequency of the proposed design is 6.85GHz and its insertion loss at the center frequency is less than -1dB. The passband of the designed filter is uniformly flat.

Figure 3 shows the snapshot of the realized filter. The proposed ultra-wideband bandpass filter is realized on TLX-8 Taconic substrate with dielectric constant of 2.55 and a thickness of 0.5mm. The size of the filter is compact.

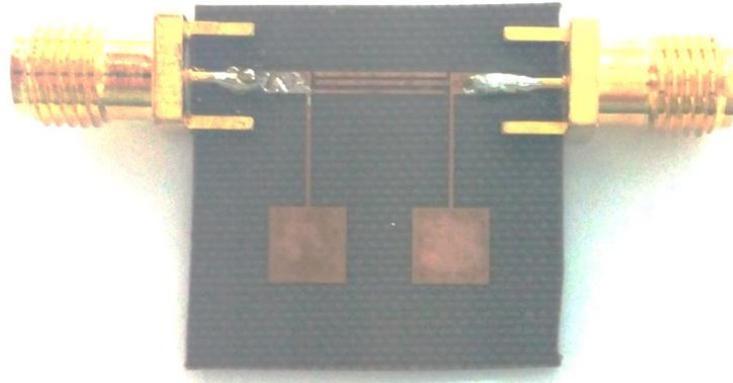


Figure 3. Photograph of the prototype filter

Figure 4 shows the experimental result of the prototype filter. The filter response is verified by a Vector Network Analyzer (model: N5230A PNA-L). It can be seen from Figure 4, the passband of the filter is not flat and considering the 10dB bandwidth, it covers from 3.2GHz to 9GHz.



Figure 4. Experimental result of the developed filter

The experimental and simulation combined results are shown in Figure 5. Comparing the CST simulation result with the prototype filter, the lower cutoff frequency has increased about 3% and the upper cutoff frequency has decreased about 15% in the realized filter. The reason of the different bandwidth, as well as the cutoff frequencies, is due to the fabrication impairments of the filter. There might be some corrossions in the surface of the strips as well as in the ground plane of the filter which might take place during the etching process that affected the results.

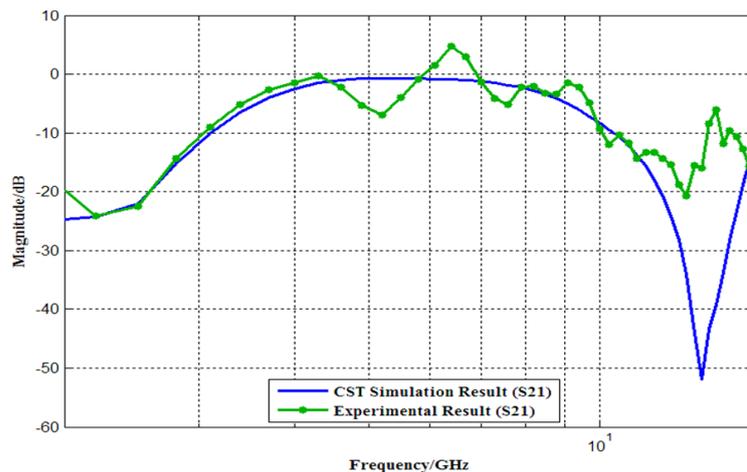


Figure 5. Experimental and CST simulation combined results

4. CONCLUSION

This paper presents the design and implementation of a compact quarter wavelength UWB bandpass filter. The filter is designed using the interdigital coupled lines, two shunt stubs and two squared pads. The interdigital line filter used three fingers; two of which are connected with the input and output transmission lines and the third one is free that is, it is not connected with anything. The -10dB passband of the filter is not completely flat; however, it can be improved by adjusting the degree of coupling. This filter has a compact size and can be used for high-speed communication devices. The passband response of the filter is within the UWB frequency range and does not make interference with another band of frequency. In order to improve the passband response and sharp transition between the passband to the stopband, more finger can be added and by adjusting the spacing and widths of the fingers

ACKNOWLEDGEMENTS

This research has been supported by the Malaysian Ministry of Science and Technology through the Science Fund under the project ID: SF14-010-0060.

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