Control Strategy for Three Phase Shunt Active Power Filter with Minimum Current Measurements

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Abstract

The active power filter has been proved to be an effective method to mitigate harmonic currents generated by nonlinear loads as well as to compensate reactive power. The methods of harmonic current detection play a crucial part in the performance of active power filter (APF). This paper presents a new control strategy in which two shunt active power filter configurations are developed in order to define new simple control algorithm which requires minimum number of current measurements. The effectiveness of the proposed control strategies are demonstrated through results. The proposed systems are implemented with MATLAB/SIMULINK. The simulation results are presented for two control strategies and comparison is made among them.

Keywords: Harmonics, Active power filter, current sensors, power qualityinprovement

1. Introduction

The increasing use of solid-state power-conversion equipment (rectifiers, inverters, cycloconverters) and other power electronic-type devices (voltage controllers, motor-speed controllers) on distribution systems is causing utilities to become much more concerned about voltage and current harmonic levels[1,2]. The nonlinear characteristic of the power semiconductors results in serious harmonics and reactive power pollution in power system[3.4]. The effective methods for harmonic suppression and reactive power compensation are more and more needed. The Passive Power Filter (PPF) is a traditional way for harmonic suppression, which is composed of power capacitor, power inductance and resistance. PPF has been regarded as the main approach in the field based on its simple architecture, little maintenance and well-developed design. But there are several disadvantages existing in PPF:1) filtering characteristic depends on the impedance of the power supply;2) the impedance characteristic is deteriorated with the frequency reduce to below the lowest resonance frequency;3) PPF can not filter the non-characteristic harmonic currents as well as to compensate for reactive power [5,6]. Principally, the active power filter operates by detecting harmonic current to calculate the amount of the compensating current needed for feeding back to the power system in the opposite direction of the harmonic current[7,8].

In the conventional p-q theory based control approach for the shunt APF, the compensation current references are generated based on the measurement of load currents and the current feedback from the shunt APF output is also required and therefore, minimum four current sensors are desired in a balanced system[9,10].

In this paper, in order to simplify the control scheme for the three phase sunt active power filter, two types of configurations for are developed based on single current measurement. One control scheme based on measurement of load current only, and other control scheme based on measurement of source current only.

2. Proposed control startegies

Basic principle of shunt active power filter is showed in Fig.1. Shunt active power filter is mainly composed of harmonic current detecting circuit and compensation current generationcircuit and is parallel connected with thenon-linear load. Its working procedure is as following: firstly the current of the load $i_L(t)$ is detected, and its harmonic component is then calculated by the harmonic current detecting circuit. The inverter is controlled to output the compensation current whose polarities are inversed with the harmonic currents. According to the formula for power line current calculation $i_s(t) = i_L(t)+i_c(t) = i_L(t)-i_{Lh}(t)$, the fundamental frequency component of power line current is left only. If the reactive power compensation is demanded additionally, the only procedure to add is to compute the reactive power component together with the calculation of harmonic component. Consequently, the unity power factor can be realized.

In the conventional p-q theory based control approach for the shunt APF, the compensation current references are generated based on the measurement of load currents and the current feedback from the shunt APF output is also required and therefore, minimum four current sensors are desired in a balanced system. In order to simplify the control scheme, two types of control techniques are developed for shunt active power

filter based on single current measurement. One control scheme needs only measurement of load current, and other control scheme needs only measurement of source current.

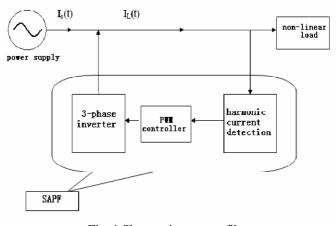


Fig. 1 Shuntactive power filter

2.1 Active Power Filter with Load Current Detection

Active power filter with load current detection only requires load current, source voltage and capacitor voltage. The control system acts in order to perform an indirect regulation of source currents, which must be sinusoidal and in phase with the corresponding line to neutral voltages. Here indirect regulation of the source current is achieved by introducing a closed loop control of the "filter flux", defined as the time integral of the filter voltage [6]. The block diagram of shunt active power filter with load current measurement is shown in Fig 2.

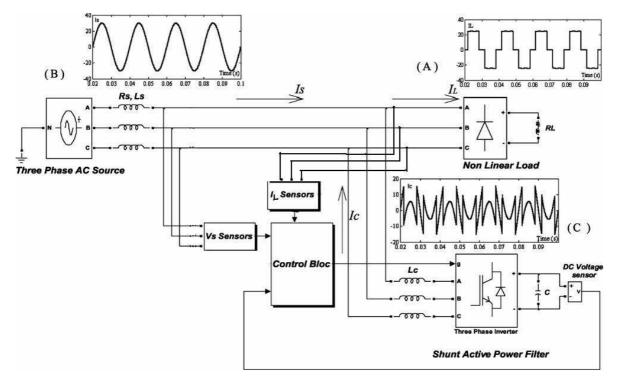


Fig.2 A.P.F with load current detection

The voltage equation for the shunt active power filter is given as

$$V_{\rm S} = V_{\rm F} + L \frac{\rm di_c}{\rm dt} \tag{1}$$

The integration of equation (1) leads to the following "flux equation".

$$\varphi_F^* = \varphi_S - \mathrm{Li}_c^*$$
(2)

Where ϕ_F^* is the reference "filter flux" and ϕ_S is the actual "source flux". The reference filter current is given by

$$i_{C}^{*} = I_{S}^{*} - I_{L}$$
 (3)

Where I_L is the measured load current and I_S^* is the reference source current. I_S^* is obtained by the equations

$$i_{sa}^{*}(t) = I_{sm} \sin (wt)$$

$$i_{sb}^{*}(t) = I_{sm} \sin (wt - 120^{0})$$

$$i_{sc}^{*}(t) = I_{sm} \sin (wt + 120^{0})$$
(4)

and I_L is directly measured by current sensors. For balanced load condition two current sensors are used for measuring load current. Equation (2) is used for calculating reference flux ϕ_F^* . The actual value of ϕ_S is obtained by integrating the output filter voltage, which can be determined on the basis of the dc voltage V_c and the inverter switch states S_A , S_B , S_C .

$$\mathbf{v}_{\rm F} = \frac{2}{3} \mathbf{V}_{\rm C} (\mathbf{S}_{\rm B} + \mathbf{S}_{\rm B} \mathbf{e}^{j\frac{2\pi}{3}} + \mathbf{S}_{\rm B} \mathbf{e}^{j\frac{4\pi}{3}}) \tag{5}$$

In this way, the non idealities of voltage source inverter (switching voltage drop and dead times) are neglected leading to steady state errors but avoiding the use of additional wide bandwidth voltage transducers to sense the voltage source inverter output voltage. The difference between reference filter flux and actual filter flux is given to the PWM controller. PWM controller generates firing pulses to control voltage source inverter. Current controlled voltage source inverter is used to inject a compensating current in to the system to relieve the supply from harmonic and reactive currents and enhance power quality indices. The shunt active power filter with load and filter current measurement is requires to measure load currents and the current feedback from the shunt active power filter therefore minimum four current sensors are desired in a balanced system. For unbalanced system six current sensors are required. Furthermore, power full microprocessors are necessary for the online evaluation of the harmonic content of the load currents. The shunt active power filter with load current detection only not requires to measure compensation current and source current and the reference source current is generated based on regulation of capacitor voltage by using PI controller. So shunt active power filter with load current detection is low cost and easy to implement.

2.2 Active Power Filter with Source Current Detection

Active power filter with source current detection only measures source current, source voltage and capacitor voltage. The basic compensation principle of a shunt APF is shown in Figure 3. It is controlled to draw/supply a compensating current Ic from/to the system, so that it cancels current harmonics on AC side, and makes the source current in phase with the source voltage. The different waveforms are shown in Fig 3. Curve A is the non-linear load current waveform and curve B is the desired mains current .Curve C shows the compensating current injected by the active filter containing all harmonics, to make mains current sinusoidal.

The voltage equation for the shunt active power filter is given as

$$V_{\rm S} = V_{\rm F} + L \frac{\rm di_c}{\rm dt} \tag{6}$$

The source current for the shunt active power filter is given as

$$I_s = I_C + I_L \tag{7}$$

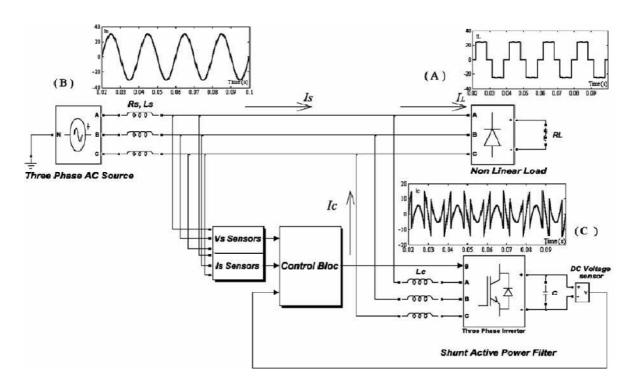
Being the rate of change of the filter current usually higher than that of the load current, equation (6) can be written as

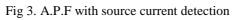
$$V_{\rm F} = V_{\rm S} - L \frac{\rm di_{\rm S}}{\rm dt} \tag{8}$$

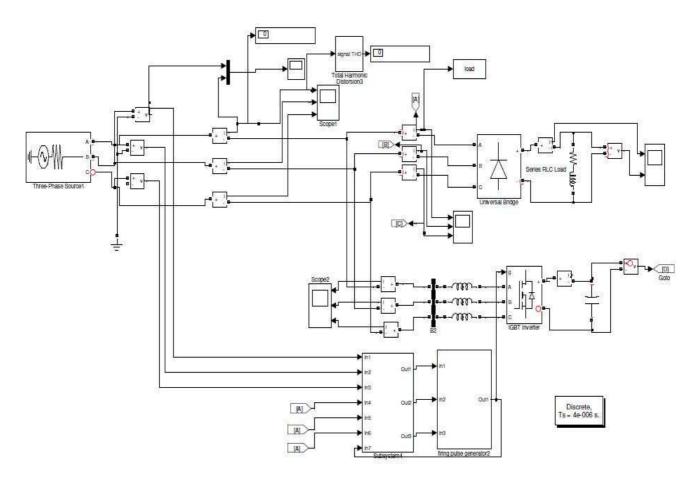
For small variations, the time derivatives can be replaced by finite differences and equation (8) can be written as

 $V_F = V_S - \tfrac{L}{\Delta t} \Delta i_S$

(9)









Where Δi_s represents the instantaneous source current error and it obtained by the equation (10)

$$\Delta \mathbf{i}_{\mathsf{S}} = \mathbf{I}_{\mathsf{S}}^{*} - \mathbf{I}_{\mathsf{S}} \tag{10}$$

Where I_s is the measured source current and I_s * is the reference source current. I_s * is obtained by the equation (10) and I_s is directly measured by current sensors. For balanced load condition two current sensors are used for measuring source current. The difference between reference source current and actual source current is given to the hysteresis controller. Hysteresis controller generates firing pulses to control inverter. Current controlled voltage source converter (VSC) is used to inject a compensating current in to the system to relieve the supply from harmonic and reactive currents and enhance power quality indices. In shunt active power filter with load and filter current measurement the compensation current references are generated based on the measurement of load currents and the current feedback from the shunt APF output is also required and therefore, minimum four current sensors are desired in a balanced system. The shunt active power filter with source current is generated based on regulation of capacitor voltage by using PI controller. So shunt active power filter with source current detection is low cost and easy to implement. Implementation of shunt APF with load current detection is done with Matlab/Simulink and it it is shown in Fig.4

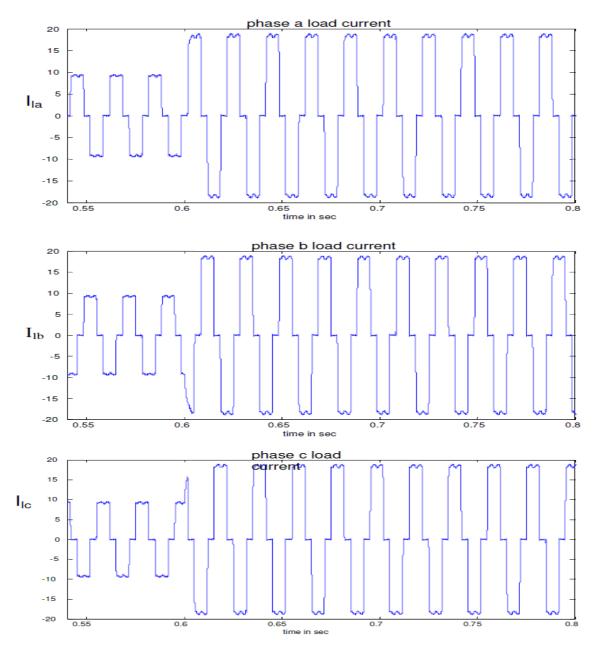
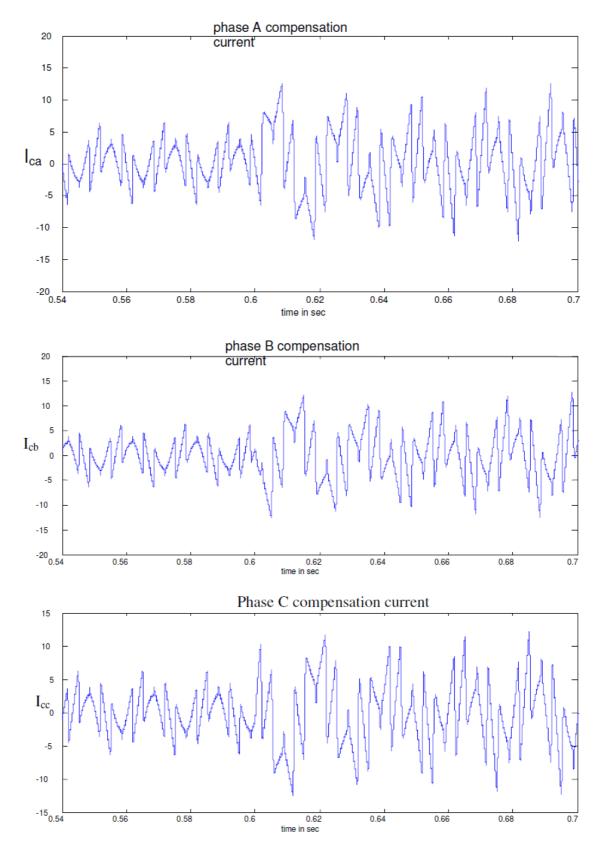


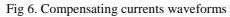
Fig 5 Three phase load current waveforms

3. Results and Analysis

3.1 Shunt APF with Load current detection

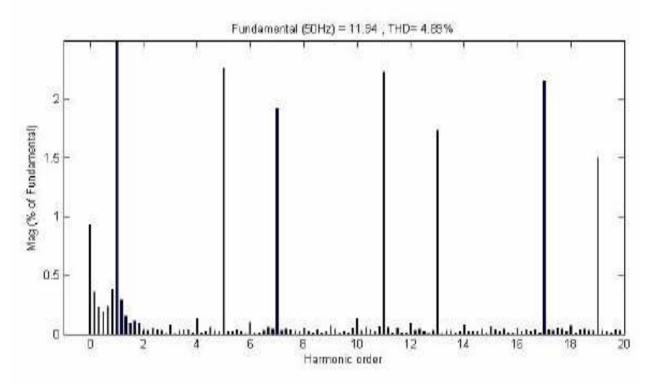
The system shown in Fig 2 is simulated in Matlab/Simulink and the Simulink diagram is shown in Fig.4. The load current containing harmonics is shown in Fig 5.

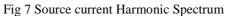




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This harmonics are eliminated by injecting compensation currents at PCC. The compensation currents are shown in Fig 6. The compensation currents supply harmonic currents and reactive power demand of the load. Total Harmonic Distortion of the Source current is reduced to 4.89%. Harmonic spectrum for source current after compensation is shown in Fig 7. From Fig 8, it is noticed that the source current is in phase with source voltage and power factor is close to unity. The source current is close to fundamental sinusoid, showing that harmonic current is eliminated from the source current. From Fig 9, it is very clear that the D.C side capacitor voltage is remains constant at its value.





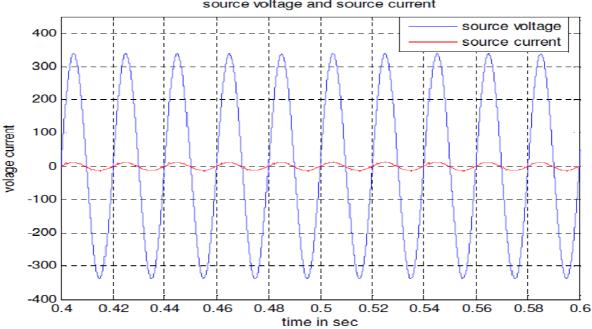




Fig 8 Source voltage and source current wave form

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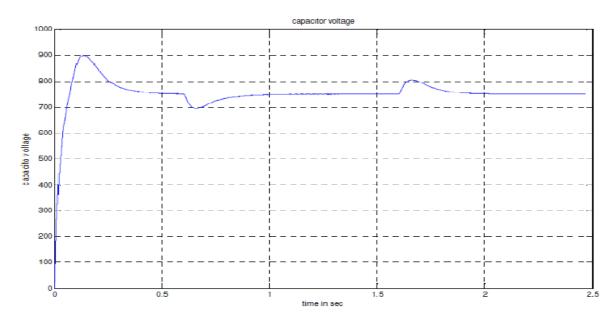


Fig 9 capacitor voltage

3.2 Shunt APF with Source Current Detection

The system shown in Fig 3 is simulated and results are presented. The load current containing harmonics are eliminated by injecting compensation currents at PCC. The compensation currents are shown in Fig 10. The compensation currents supply harmonic currents and reactive power demand of the load. Harmonic spectrum for source current after compensation is shown in Fig 11. The source current Total Harmonic Distortion is reduced to 3.20%.

The source current waveform is close to fundamental sinusoid, showing that harmonic current is eliminated from the source current and also the power factor is close to unity. The source current is in phase with source voltage and is shown Fig 12. The voltage across the D.C side capacitor is also shown in Fig 13.

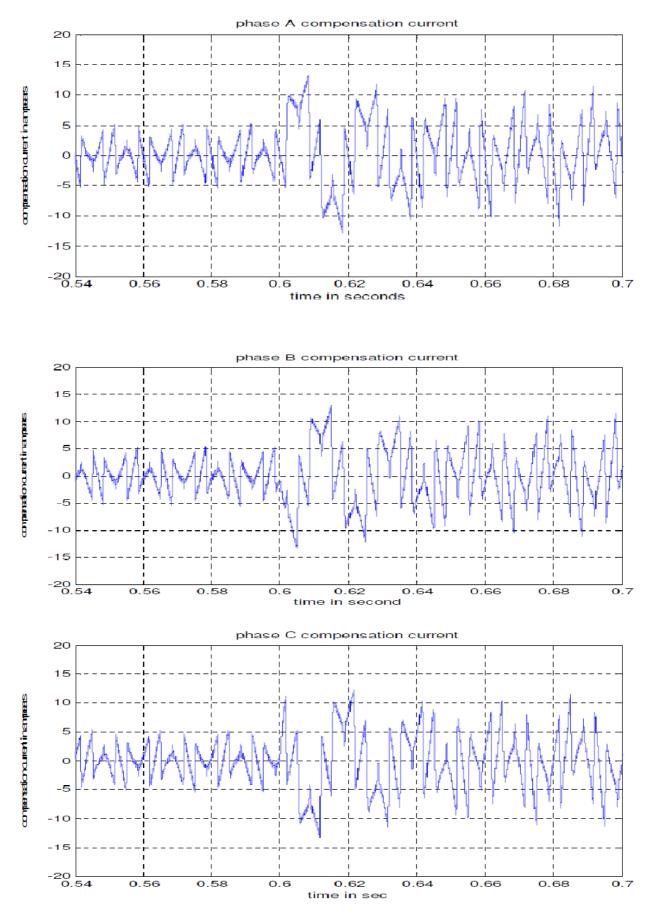
TYPE	%THD for 10A	%THD for 20A	Number of current sensors for balanced load	Number of current sensors for unbalanced load
Without Active	28.22	29.8		
Power Filter				
Load current detection	4.89	6.9	2	3
Source current detection	3.20	5.7	2	3

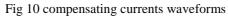
Table 1. Comparison of %THD in source current and required current sensors

4. Conclusion

Control methods of shunt active power filter with minimum measurement requirements are discussed in this chapter. One control scheme is based on measurement of load current only and other control scheme is based on source current only. These Active power filters are used to eliminate harmonic currents as well as to compensate reactive power of the load. The technique is used in this work is easy to implement, and requires less number of current sensors and transformations.

Shunt active power filter with source current detection and shunt APF with load current measurement are investigated and the corresponding results are compared with each other and it is observed that the shunt active power filter with source current measurement exhibits superior performance. The steady state and dynamic responses of the shunt active power filter with source current measurement is better than the APF with load current measurement





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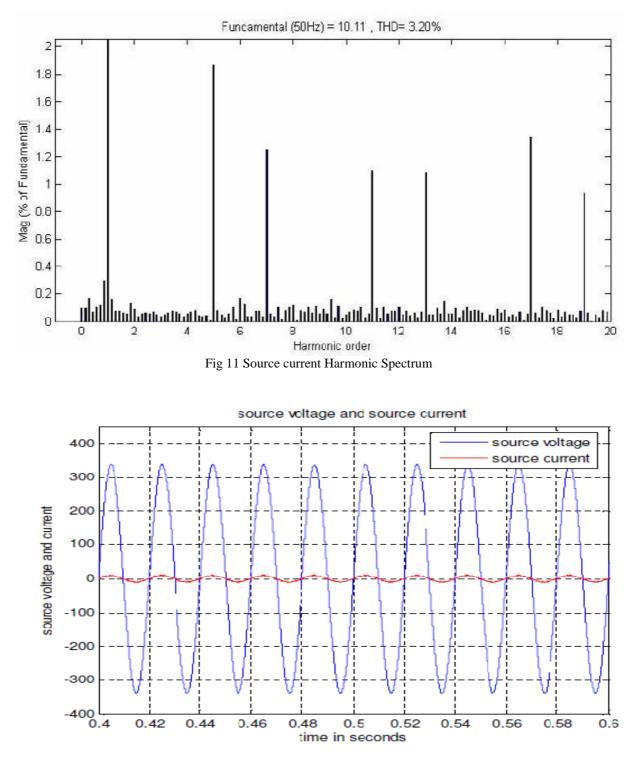


Fig 12 Source voltage and source current wave form

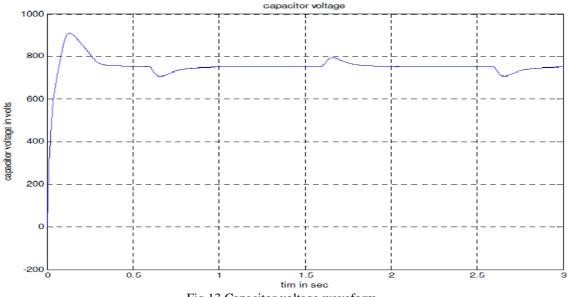


Fig 13 Capacitor voltage waveform

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