Impedance Matching Improvement of Half-Cut Broadband Printed Monopole Antenna with Microstrip Feeding

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Article Info	ABSTRACT
Article history:	The requirement of wireless access networks and user equipments to support coexistence of many communication standards and frequency bands poses challenge on antenna to be broadband and small. The application of half-cut technique to broadband printed monopole with microstrip feeding worsens the resulted antenna's impedance. To improve the half-cut antenna impedance matching, two methods were investigated in this paper: (1) monopole and ground extension, (2) the application of microstrip line transformer and ground extension. The first approach only produces limited improvement, whereas method #2 can enhance the return loss significantly. The second approach potentially produces antenna pair that has low mutual coupling, good return loss, and small size. Considering its radiation pattern, the antenna is suitable for diversity and MIMO. Its application in broadband microwave-photonic access point need special arrangement due to radiation null at 5 GHz band at right side.
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1. INTRODUCTION

Current and future wireless access network and user equipment are required to support the coexistence of many communication standards and operating frequencies (bands). More functionalities and hardwares should be packed in the limited space. In the antenna context, these requirements pose challenges on producing antenna that covers very wide range of frequency and at the same time only takes small space.

In this respect, broadband printed monopole antenna which is aimed to cover 1.7 - 6.0 GHz has been proposed and miniaturized [1] using half-cut technique. This miniaturization method has been used successfully in various types of antennas [2-6] in which impedance bandwidth and radiation pattern of original antennas commonly can be retained. However, the application of the technique in [1] raises two problems: (a) the microtrip line impedance is changed from 50 Ohm to 90 Ohm hence the antenna's return loss characteristic worsen, (b) the radiation pattern is deformed especially at 5 GHz band.

This paper is intended to improve the impedance characteristics of half-cut printed rectangular monopole antenna with microstrip feed line [1]. Two approaches are investigated, i.e. (1) the use of monopole and/or ground extension, (2) the utilization of line transformer between the miniaturized monopole and the port. The half-cut technique is applied to bandwidth-enhanced printed rectangular monopole [7] which is constructed on 1.6mm-thick FR4 ($\varepsilon_r = 4.4$), width of 48 mm and length of 69 mm.

The rest of this paper is organized as the following. Section 2 describes the research method involved in the investigation. The results of the investigations are presented and discussed in Section 3. Finally, Section 4 concludes this paper.

2. RESEARCH METHOD

Actually, [1] has tried to rectify the impedance mathing problem by extending its ground 3 mm. Although the return loss characteristics can be improved, the $|S_{11}|$ values are still quite close to -10 dB at quite large portion of the antenna's intended frequency range, i.e. from 2.3GHz to 4.7 GHz. Provided that the half-cutting line affects the impedance, the extension of monopole and ground need to be investigated further to find optimum extension configuration.

Another insight from impedance characteristics of half-cut antenna (without ground extension) in [1] is that its |S11| graph is very good if calculated with reference impedance of 90.5 Ohm. This inspires the possibility of using microstrip line impedance transformer between the monopole which is round 90.5 Ohm the the port which is required to be 50 Ohm.

The investigations of the two approaches are conducted by employing electromagnetic simulation software, CST Microwave Studio (CST-MWS). Time domain solver is employed with accuracy is set to -50 dB. Moreover, all of $|S_{11}|$ calculations are normalized to 50 Ohm; if not set like this, CST MWS reports $|S_{11}|$ values which are normalized to the antenna's port impedance that sometimes are not 50 Ohm.

The following two sub-sections explain the details.

2.1. Monopole and Ground Extension

Variables being investigated are described in Figure 1. Half-cut line divides the original antenna exactly into two halves, right-half and left-half. Only left-half is presented in Figure 1. Extending the ground of left-half antenna means adding its ground-width to right-direction along W_{ext} or W_{eg} mm. Similarly, monopole extension of the left-half is adding the width of the monopoleand the feedline to right-direction along M_{ext} mm. Combination of ground and monopole extensions are also investigated.

2.1. Microstrip Line Impedance Transformer

Figure 2 describe the impedance transformer. The width of half-cut monopole's feeding line is 1.6 mm, whereas the original antenna's feed line width is 3.2 mm to produce characteristic impedance of 50 Ohm. In this arrangement, the antenna port is specified having impedance of 50 Ohm with length of 3 mm. The variable is the length the transformer line (L_{trafo}) started from the edge of the 50 Ohm microstrip transmission line. L_{trafo} determines rate of change of impedance. Smoother the impedance changes, better is the impedance matching.

3. RESULTS AND ANALYSIS

Results from two types of investigations are presented in the following sub-sections. Then, one design which produces the best $|S_{11}|$ is chosen to show its radiation pattern characteristics.

3.1. Monopole and Ground Extension

Variation of $|S_{11}|$ as effect of varied M_{ext} values at a fixed W_{ext} is presented in Figure 3. Figure 4 shows the effect of varying W_{ext} at a fixed value of M_{ext} to the antenna's $|S_{11}|$ values. It is clear that extending the width of monopole and feedline only worsen the antenna's $|S_{11}|$ as proved by Figure 3. Improvement on the return loss characteristics is demonstrated by Figure 4 in which W_{ext} up to 2 mm produces significant decrease of return loss. However, the effect of increasing W_{ext} larger than 3 mm only improves $|S_{11}|$ slightly.

In general, both M_{ext} and W_{ext} affect return loss. M_{ext} is stronger than W_{ext} . Unfortunately M_{ext} cannot create return-loss enhancement. On other side W_{ext} influence is only limited to 3 mm.

3.2. Microstrip Line Impedance Transformer

Antenna configuration depicted in Figure 2 is investigated in term of its transformer length and ground extension. As shown in Figure 5, |S11| is improved with the increase of L_{trafo} ; the more gradual the impedance changes, the better is the impedance matches. The maximum improvement is at $L_{trafo} = 26.67$ mm. At traformer length of 30 mm, the return loss is slightly worse than 26.67 mm; maybe the EM field configuration at the lower part of the monopole is disturbed by the transformer upper end.

It can be observed that $|S_{11}|$ curves in Figure 5 are very similar. This similarity is determined by at W_{eg} ; the reflection coefficient curves of the same W_{eg} but different L_{trafo} follow similar shape; the curves of the same L_{trafo} but different W_{eg} follow quite different trends, see Figure 6. Therefore, W_{eg} determines the curve shape and L_{trafo} scale the magnitude of S_{11} .

Nonetheless, it does not mean that we should choose W_{eg} and then adjust L_{trafo} to get the optimum result. In the contrary, it has been known from these simulations, see Figure 5, that $L_{trafo} = 26.67$ mm produces the lowest $|S_{11}|$ at W_{eg} values being simulated. Therefore, the optimization process is actually choosing W_{eg} values of $L_{trafo} = 26.67$ mm that results the optimum $|S_{11}|$ curve shape. As an example, Figure 6

offers trade off between 2 – 3 GHz or 3.5 GHz band. If 3.5 GHz band is considered more important than 2 – 3 GHz, then $W_{eg} = 0.8$ mm should be chosen. However, in case of 2 – 3 GHz band is more critical, higher value of W_{eg} can be chosen; if 5 GHz band is also considered, $W_{eg} = 1.85$ or 2.9 mm may give better performance.

3.3. Discussion

Section 3.1 describes that playing monopole and/or ground extension only provides limited space in improving return loss of the half-cut antenna. Fortunately, the second method investigated in this paper produce much better $|S_{11}|$ enhancement. The success of the characteristic impedance transformation technique confirms that the application of half-cut method to the printed monopole double the impedance of the antenna, i.e. 50 Ohm (original antenna) to 90.5 Ohm (half-cut antenna). It also implies that the half-cut antenna's impedance is quite stable (or homogeneous) along the (half-cut) transmission line hence the microstrip transformer works well from 10 mm to 30 mm (simulation results of L_{trafo} below 20mm are not presented in this paper, but they follow similar trend).

Investigation on left-right half-cut antenna pair compared to original antenna pair in [8] shows that original pair is preferred due to its better return loss characteristics although left-right pair produces better mutual coupling. The application of microstrip transformer may produce better antenna pair for broadband microwave-photonic access point (BMwPhAP), diversity, or MIMO due to its lower mutual coupling while retaining potentially good return loss.

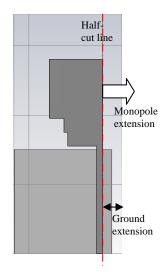


Figure 1. Description of monopole and ground extensions effect on the half-cut antenna's $|S_{11}|$

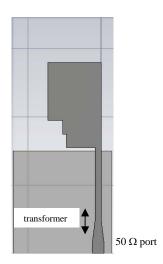


Figure 2. Arrangement of microstrip 50 Ohm port, transformer, ground extension, and half-cut antenna

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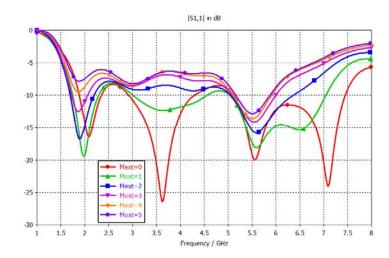


Figure 3. $|S_{11}|$ at $W_{\text{ext}} = 3$ mm, with monopole and feedline width is extended from 0 to 5 mm.

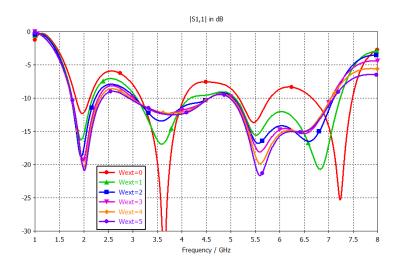


Figure 4. $|S_{11}|$ at $M_{\text{ext}} = 1$ mm, with ground width is extended from 0 to 5 mm.

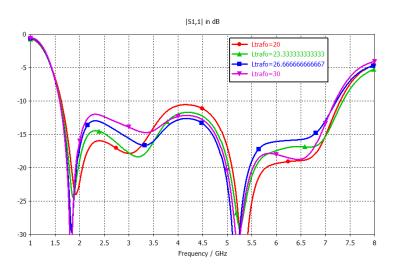


Figure 5. $|S_{11}|$ at $W_{eg} = 0.8$ mm, with ground width is extended from 20 mm to 30 mm.

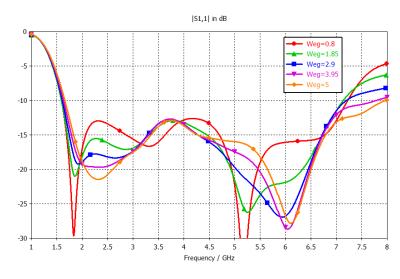


Figure 6. $|S_{11}|$ at $L_{\text{trafo}} = 26.67$ mm, with ground width is extended from 0.8 mm to 5 mm.

Considering that 2 - 3 GHz and 5 GHz bands as priority, left half-cut antenna with $W_{eg} = 2.9$ mm and $L_{trafo} = 26.67$ mm is chosen as the best candidate. This simulated antenna radiation pattern is depicted in Figure 7. Up to 3.5 GHz, the radiation pattern is nearly omnidirectional. Nonetheless, the antenna has null at right side. While its return loss is good at 1.7 - 6.0 GHz, the antenna needs special arrangement if used at 5.8 GHz due to it null in radiation pattern at that band. With this radiation pattern characteristics, this antenna is suitable for diversity and MIMO.

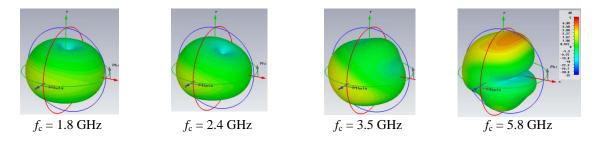


Figure 7. 3D realized gain pattern of left-half antenna with $L_{\text{trafo}} = 26.67$ mm and $W_{\text{eg}} = 2.9$ mm.

4. CONCLUSION

Half-cut technique can miniaturize symmetrical printed antenna into 50% of original size. However, its application to microstrip-fed printed monopole antenna worsens the antenna impedance hence matching enhancement method is needed. This paper has investigated two approaches: (1) monopole and ground extension, (2) microstrip line transformer and ground extension. Method #1 only produces limited improvent to return loss characteristic of half-cut antenna. Method #2 can enhance the impedance matching significantly. The length of the line transformer the major factor in reducing $|S_{11}|$, whereas the the ground extension plays tradeoff among frequency band being optimized. This result potentially implemented in left-right half-cut antenna pair to used in broadband microwave photonic access point, diversity, or MIMO which not only provide good isolation between antenna in pair but also has good return loss characteristics. The antenna's radiation pattern is nearly omnidirectional at frequency up to 3.5 GHz but exhibit nulls at 5 GHz band. Hence, it is suitable for diversity and MIMO but needs additional arrangement if it is used in access point.

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